Modern Academy For Engineering for Engineering& Technology in Maadi

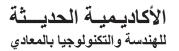




Sample Course File

Modern Academy For Engineering for Engineering& Technology in Maadi

odern



Basic Course Documents (By-Law 2000)

Course Code: M578, Title: Hydraulic Power Systems

\checkmark	Course Specifications
\checkmark	Lecturers Resume
\checkmark	Assistants Resume
✓	Lecture notes/text book
✓	Laboratory Book

✓=Document Exists x=Document doesn't exist NR=Not Relevant

Modern Academy For Engineering for Engineering& Technology in Maadi



الأكاديمية الحديثة للهندسة والتكنولوجيا بالمعادي

Course Specifications M578: Hydraulic Power Systems

A- Affiliation

Relevant program: Department offering the program: Department offering the course: Date of specifications approval: B - Basic information Title: Hydraulic Power System Teaching Hours: Manufacturing Engineering and Production Technology BSc Program Mechanical Engineering Department Mechanical Engineering Department September 2015

Code: M578 Lectures: 3 Practical: 2 Year/level: Fifth/first Semester Tutorial:2 Total: 7

C - Professional information

1 – Course Learning Objectives:

By the end of this course the students should demonstrate the knowledge and understanding of the construction and operation of hydraulic power systems and their basic elements. They should be able to operate, maintain, design, calculate and analyze the performance of hydraulic power systems and their basic components.

2 - Intended Learning Outcomes (ILOS)

a - Knowledge and understanding:

On successful completion of the course, the student should demonstrate knowledge and understanding of:

- a1- Classification and specifications of power systems (A3, A8)
- a2- Theoretical background needed to calculate and analyze the characteristics of the hydraulic systems and their components (A1, A2).
- a3- Basic properties of hydraulic fluids and their effect on the system performance (A3)
- a4- Construction, operation and characteristics of the basic components of hydraulic power systems; pumps, valves, actuators, transmission lines and accessories (A3, A3)).
- a5- Standard symbols of hydraulic power systems (A3)
- a6- Procedures of design of the hydraulic systems using industrial elements(A4,A5)
- a7- Computer software related to hydraulic power systems design, calculation and animation (A1, A4).

b - Intellectual skills:

On successful completion of the course, the student should be able to.

- b1- Investigate the effect of hydraulic fluid properties on the function of hydraulic power systems (B1, B13)
- b2- Deduce mathematical relations describing the steady state performance of hydraulic power systems and their elements and select the proper methods for their solution (B1, B2, B13)
- b3- Analyze the static characteristics of hydraulic power systems and their components (B5, B9, B14)
- b4- Classify and compare the different ways of hydraulic elements connection (B2,B5,B15).

c - Professional and practical skills:

- On successful completion of the course, the student should be able to:
- c1- Design, assemble, operate, test and maintain simple hydraulic system (C1,C3)
- c2- Calculate the steady state characteristics of hydraulic systems and their subsystems and basic components and (C1, C5).
- c3- Use computer software; Automation Studio, Marex and other available programs to design, calculate, simulate or animate hydraulic power systems and their components (C5).
- c4- Solve limited operational problems related to the hydraulic power systems and their basic elements (C1, C5,C6).
- c5- Use experimental facilities to visualize and investigate the cavitation phenomenon and evaluate the characteristics of typical roto-dynamic and displacement pumps (C12, C16, C17).
- c6- Use experimental facilities to assemble and operate diverse hydraulic circuits (C17).

d - General and transferable skills:

On successful completion of the course, the student should be able to:

- d1- Work in a team and involve in group discussion and seminars (D1, D3).
- d2- Communicate effectively and present data and results orally and in written form (D3).
- d3- Use ICT facilities in presentations (D4).
- d4- Search for information's in references and in internet (D7).
- d5- Practice self-learning (D7, D9).

Course Contribution in the Program ILO's

ILO's		Program ILO's
А	Knowledge and understanding	A1, A2, A3, A4, A5, A8
В	Intellectual skills	B1, B2, B5, B9, B13, B14, B15
С	Professional and practical skills	C1, C3, C5, C6, C12, C16, C17
D	General and transferable skills	D1, D3, D4, D7, D9

3 - Contents

Торіс	Lecture hours	Tutorial hours	Practical hours
Power systems, classification, operation, and comparison.	2		
Introduction to hydraulic power systems and standard symbols	2	2	2
Hydraulic fluids; properties and their effect on the system performance.	4	2	2
Hydraulic transmission lines and connectors	2	2	2
Hydraulic pumps:		4	4
 Classification and basic mathematical relations 	2		
 Gear pumps, vane pumps and piston pumps 	4		
Fixed and variable displacement pumps and pump control	2	2	2
Control valves		2	2
 Classification and basic design 	2		
• Pressure control valves (direct/pilot operated); relief valves, pressure			
reducers, sequence valves and accumulator charging valves	4	2	2
Directional control valves	2	2	2
 Flow control valves 	2		
Check valves	2		
Hydraulic actuators; cylinders, motors and rotary actuators	2	2	2
> Accessories; accumulators, filters, reservoirs, pressure switches,etc	2	4	2
Case studies; design and analysis of function of hydraulic circuits of industrial and mobile systems.	2		6
Mini project; design and analysis of the hydraulic system for an industrial application. Analysis of the possible operational problems	6	4	2
> Seminar	3	2	
Total hours	45	30	30

4 - Teaching and Learning and Assessment methods:

Course ILO's		Teaching Methods				Learning Methods		Assessment Method						
		Lecture	Presentations & Movies	Discussions & seminars	Tutorials	Problem solving	Laboratory & Experiments	Researches & Reports	Modeling and Simulation	Written Exam	Practical Exam	Quizzes	Term papers	Assignments
eta	a1	1	1	1	1		1	1		1		1	1	
Knowledg e & Lindoreto	a2	1			1					1		1	1	1
u N N	a3	1			1					1		1	1	1

					r						1			
	a4	1	1	1	1	1	1	1		1		1	1	1
	a5	1					1			1	1	1	1	1
	a6	1						1					1	1
	a7	1		1	1	1		1	1				1	
al	b1	1			1					1		1		1
ellectu Skills	b2	1			1	1				1		1	1	1
Intellectual Skills	b3	1	1	1	1		1	1		1	1		1	
Ē	b4	1	1		1		1	1		1	1	1	1	1
<u>s</u>	c1	1	1		1	1	1			1	1	1	1	1
Ski	c2	1			1					1		1	1	1
lied nal	c3	1		1		1		1	1				1	1
Applied Professional Skills	c4	1			1	1					1		1	1
ofe	c5						1				1			
٦ ۲	c6						1				1			
Ŀ.	d1			1		1		1					1	
Trai	d2		1	1				1	1				1	
ieral T Skills	d3	1	1					1					1	1
General Tran. Skills	d4	1	1	1				1						
G	d5							1	1				1	

5- Assessment Timing and Grading:

Assessment Method	Timing	Grade (Degrees)
Semester Work: seminars, quizzes assignments and reports	Bi-Weekly	15
Mid-Term Exam	6-th Week	15
Practical Exam	Fifteenth week	20
Written Exam	Sixteenth week	100
Total		150

6- List of references:

- 6-1 Course notes: Non
- 6-2 Required books
 - M Galal Rabie, Fluid Power Engineering, McGraw-Hill. NY, 2009
- 6-3 Recommended books: Non
 - M Galal Rabie, Automatic Control for Mechanical Engineers, ISBN 977-17-9869-3, 2010
 - Ibrahim Saleh and M Galal Rabie, Fluid Mechanics for Engineers, ISBN 978-977-5092-00-7, 2011

6-4 Periodicals, Web sites, etc.

http://www.moog.com/, http://www.boschrexroth.com/en/xc/, http://www.norgren.com/global/ http://www.eaton.com/Eaton/index.htm http://www.nfpa.com/

7- Facilities required for teaching and learning:

- Fluid Power Lab.
- Computer, Data show and Computer programs; Automation studio, Marex, Rexroth hydraulic trainer, Rexroth hydraulic element animation and TK-Solver.

Course coordinator:	Prof. Dr. M Galal Rabie
Head of the Department:	Dr. Abdelmegid Abdellatif
Date:	September 2015

Lecturers Resume

أستاذ دكتور / محمود جلال الدين محمد ربيع؛ قائم بأعمال وكيل الأكاديمية للتعليم والطلاب Name: Mahmoud Galal El-Din Mohamed RABIE Birth date and place: April 19, 1946, Dakahlia, Egypt Email: Galalrabie@hotmail.com Telephone: +20100 2211546 Address: 33 A Elbably st., 11331, Hadayek Elkobbah, Cairo, Egypt Education: PhD Specialization: Applied Computing and Automation Systems for Industry and Management Awarded by: Claude Bernard University Lyon 1 and INSA, Lyon, France, Oct. 1980 Diploma Specialization: (DEA) Mechanical Engineering Awarded by: Claude Bernard University Lyon 1, France, Nov., 1978 MSc **Specialization:** Mechanical Engineering Awarded by: Military Technical College, Cairo, Egypt, Jan. 1977 BSc **Specialization:** Mechanical Engineering (Aircraft Engines) Awarded by: Military Technical College, Cairo, Egypt, April, 1968 **Positions Occupied and work experience**

- Professor of Mechanical Engineering, Military Technical College (MTC), Nov. 1991
- Head of the Aircraft Mechanical Dpt.; MTC, Head of the Specialized Mechanical Engineering Branch, MTC, • Chairman of the Scientific Council of the Aeronautical Department; MTC, Member of the Scientific Committee and Scientific Council of the MTC, up to January, 2005
- Profound experience in the vocational training and technical consultations in fluid power.
- Rapporteur general of the international conferences on Aerospace Sciences and Aviation Technology; ASAT-6, • ASAT-7, ASAT-8 and ASAT-9, organized by the MTC, Cairo, Egypt.
- Cooperation with the National Authority for Quality Assurance and Accreditation in Education, NAQAAE, (2008-2009); Member of the High Committee for Higher Education, 2008 up-till now

Post graduate activities:

- Supervised 6 PhD and 29 MSc thesis. •
- Member of examination board and jury for MSc & PhD examinations and thesis in the faculties of engineering of ٠ Cairo, Ain-Shams, Alexandria, Zagazig, Al-Azhar and Helwan Universities, the Military Technical College, Cairo and Beihang Univ., Beijing, China..

Published Papers:

Author and co-author of 68 scientific papers, published in refereed national and international journals and conferences. Lectured Courses:

M201, M399, M482, M578, M599, MNF311, MNF413, MNF522, MNF537, MNF361, MNF362, MNF461, MNF561, -MNF563.

Authored books:

- M Galal Rabie, Fluid Power Engineering, McGraw-Hill, NY, USA, May 18, 2009.
- M Galal Rabie, Fluid Power Engineering, McGraw-Hill, NY, USA, (Korean Language Edition), 2012, ISBN-13: • 9788996621102
- M Galal Rabie, Automatic Control for Mechanical Engineers, ISBN 977-17-9869-3, 2010
- Ibrahim Saleh and M Galal Rabie, Fluid Mechanics for Engineers, ISBN 978-977-5092-00-7, 2011
- M Galal Rabie, Introduction to Aeronautics, Printed lectures and web enabled ebook, Military Technical College, • Cairo, 2011 (Lecture Notes).
- M Galal Rabie, A Allam Elsenbawy, M Metwally and Tamer Nabil, Aerospace Applications of Fluid Power, • Printed Lectures, Military Technical College, Cairo, 2011 (Lecture Notes).

Current Institution:

Vice Dean of the Modern Academy for Engineering and Technology in Maadi, Cairo, Egypt.

Published Papers	Supervised Thesis			
During the last 5 years	Total	MSc Thesis	PhD Thesis	
10	68	29	6	

Assistants Resume

م.م / يحيى محمود عبد الوهاب حسن العطار

Name: Yahia Mahmoud Abdelwahab Hassan Elattar

Birth date and place:25th January 1985, Sharkia, EgyptEmail:ymelattar@gmail.comTelephone:0100 45 75 155Address:54 Taqseem ElMesaha, Maadi, Cairo, Egypt

Education:

PhD Specialization: Mechanical Design and Production Engineering Institution: Faculty of Engineering - Ain Shams University

(NOT COMPLETED / STILL ATTENDING)

MSc Specialization: Mechanical Design and Production Engineering Awarded by: Faculty of Engineering - Cairo University Thesis title: Modeling, Simulation and investigation of Vehicle Suspension and Design of Active Controllers

BSc Specialization: Manufacturing Engineering and Production Technology Awarded by: Modern Academy for Engineering and Technology, Cairo, Egypt, 2007 Grade: Excellent with Honor Degree Graduation project Grade: Excellent

POSITIONS OCCUPIED AND WORK EXPERIENCE

Position: Lecturer Assistant From (Sep 2007) to (till now)

Institution: Mechanical Engineering Department, Modern Academy for Engineering & Technology

Teaches the following courses:

- Automatic Control
- Fluid Power Engineering Hydraulics
- Machine Tool Design
- Engineering Economy
- Engineering Drawing
- Production Engineering Workshop
- Modeling and Simulation
- AutoCAD (summer training course)

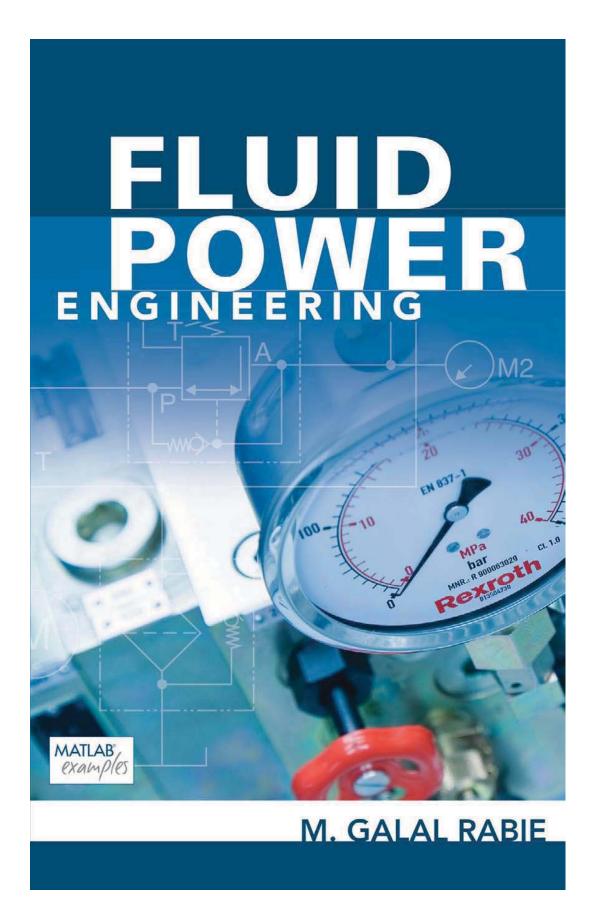
Publications

- Elattar Y. M., Rabie M.G., and Metwalli S.M., "On the Dynamics of Vehicle Passive Suspension Incorporating Twin-Tube Pressurized Shock Absorber", Proceedings of the *17th International Conference on Applied Mechanics and Mechanical Engineering, AMME-17*, MTC, Cairo, 2016
- Elattar Y. M., Metwalli S.M., and Rabie M.G., "PDF Versus PID Controller for Active Vehicle Suspension", Proceedings of the 17th International Conference on Applied Mechanics and Mechanical Engineering, AMME-17, MTC, Cairo, 2016



Basic Reference

M Galal Rabie, Fluid Power Engineering, McGraw-Hill, NY, USA, May 18, 2009.



Fluid Power Engineering This page intentionally left blank

Fluid Power Engineering

M. Galal Rabie, Ph.D. Professor of Mechanical Engineering Modern Academy for Engineering and Technology Cairo, Egypt



New York Chicago San Francisco Lisbon London Madrid Mexico City Milan New Delhi San Juan Seoul Singapore Sydney Toronto

The McGraw-Hill Companies

Copyright © 2009 by The McGraw-Hill Companies, Inc. All rights reserved. Except as permitted under the United States Copyright Act of 1976, no part of this publication may be reproduced or distributed in any form or by any means, or stored in a database or retrieval system, without the prior written permission of the publisher.

ISBN: 978-0-07-162606-4

MHID: 0-07-162606-9

The material in this eBook also appears in the print version of this title: ISBN: 978-0-07-162246-2, MHID: 0-07-162246-2.

All trademarks are trademarks of their respective owners. Rather than put a trademark symbol after every occurrence of a trademarked name, we use names in an editorial fashion only, and to the benefit of the trademark owner, with no intention of infringement of the trademark. Where such designations appear in this book, they have been printed with initial caps.

McGraw-Hill eBooks are available at special quantity discounts to use as premiums and sales promotions, or for use in corporate training programs. To contact a representative please e-mail us at bulk-sales@mcgraw-hill.com.

Information contained in this work has been obtained by The McGraw-Hill Companies, Inc. ("McGraw-Hill") from sources believed to be reliable. However, neither McGraw-Hill nor its authors guarantee the accuracy or completeness of any information published herein, and neither McGraw-Hill nor its authors shall be responsible for any errors, omissions, or damages arising out of use of this information. This work is published with the understanding that McGraw-Hill and its authors are supplying information but are not attempting to render engineering or other professional services. If such services are required, the assistance of an appropriate professional should be sought.

TERMS OF USE

This is a copyrighted work and The McGraw-Hill Companies, Inc. ("McGraw-Hill") and its licensors reserve all rights in and to the work. Use of this work is subject to these terms. Except as permitted under the Copyright Act of 1976 and the right to store and retrieve one copy of the work, you may not decompile, disassemble, reverse engineer, reproduce, modify, create derivative works based upon, transmit, distribute, disseminate, sell, publish or sublicense the work or any part of it without McGraw-Hill's prior consent. You may use the work for your own noncommercial and personal use; any other use of the work is strictly prohibited. Your right to use the work may be terminated if you fail to comply with these terms.

THE WORK IS PROVIDED "AS IS." McGRAW-HILL AND ITS LICENSORS MAKE NO GUARAN-TEES OR WARRANTIES AS TO THE ACCURACY, ADEQUACY OR COMPLETENESS OF OR RESULTS TO BE OBTAINED FROM USING THE WORK, INCLUDING ANY INFORMATION THAT CAN BE ACCESSED THROUGH THE WORK VIA HYPERLINK OR OTHERWISE, AND EXPRESS-LY DISCLAIM ANY WARRANTY, EXPRESS OR IMPLIED, INCLUDING BUT NOT LIMITED TO IMPLIED WARRANTIES OF MERCHANTABILITY OR FITNESS FOR A PARTICULAR PURPOSE. McGraw-Hill and its licensors do not warrant or guarantee that the functions contained in the work will meet your requirements or that its operation will be uninterrupted or error free.Neither McGraw-Hill nor its licensors shall be liable to you or anyone else for any inaccuracy, error or omission, regardless of cause, in the work or for any damages resulting therefrom. McGraw-Hill has no responsibility for the content of any information accessed through the work. Under no circumstances shall McGraw-Hill and/or its licensors be liable for any indirect, incidental, special, punitive, consequential or similar damages that result from the use of or inability to use the work, even if any of them has been advised of the possibility of such damages. This limitation of liability shall apply to any claim or cause whatsoever whether such claim or cause arises in contract, tort or otherwise. To my wife Fatemah Rafat

This page intentionally left blank

About the Author

M. Galal Rabie, **Ph.D.**, is a professor of mechanical engineering. Currently, he works in the Manufacturing Engineering and Production Technology Department of the Modern Academy for Engineering and Technology, Cairo, Egypt. Previously, he was a professor at the Military Technical College, Cairo, Egypt. He is the author or co-author of 55 papers published in international journals and presented at refereed conferences, and the supervisor of 24 M.Sc. and Ph.D. theses.

MATLAB and Simulink are registered trademarks of The MathWorks, Inc. See www.mathworks.com/trademarks for a list of additional trademarks. The MathWorks Publisher Logo identifies books that contain MATLAB[®] and/or Simulink[®] content. Used with permission. The MathWorks does not warrant the accuracy of the text or exercises in this book. This book's use or discussion of MATLAB[®] and/or Simulink[®] software or related products does not constitute endorsement or sponsorship by The MathWorks of a particular use of the MATLAB[®] and/or Simulink[®] software or related products.

For MATLAB[®] and Simulink[®] product information, or information on other related products, please contact: The MathWorks, Inc. 3 Apple Hill Drive Natick, MA 01760-2098 USA Tel: (508) 647-7000 Fax: (508) 647-7001 E-mail: info@mathworks.com Web: www.mathworks.com

Contents

	Prefa	ice		xix
1	Intro 1.1 1.2	Introduc The Clas 1.2.1	o Hydraulic Power Systemsetionssification of Power SystemsMechanical Power SystemsElectrical Power Systems	1 1 2 2 3
			Pneumatic Power Systems	4
			Hydrodynamic Power Systems	5
		1.2.5		6
	1.3	Basic Hy	vdraulic Power Systems	8
	1.4	The Adv	vantages and Disadvantages of	
		Hydraul	ic Systems	9
	1.5		ing Power Systems	10
	1.6	Exercise	s	11
	1.7	Nomenc	lature	13
2	Hyd	raulic Oil	s and Theoretical Background	15
	2.1		tion	15
	2.2	Basic Pro	operties of Hydraulic Oils	16
		2.2.1	Viscosity	16
		2.2.2	Oil Density	25
		2.2.3		30
		2.2.4	1	37
		2.2.5	Vapor Pressure	38
		2.2.6	Lubrication and Anti-Wear	
			Characteristics	39
		2.2.7	Compatibility	39
		2.2.8	Chemical Stability	39
		2.2.9	Oxidation Stability	39
		2.2.10	Foaming	39
		2.2.11	Cleanliness	40
		2.2.12	Thermal Properties	45
		2.2.13	Acidity	45

X Contents

		2.2.14Toxicity2.2.15Environmentally Acceptable	45
		Hydraulic Oils	46
	2.3	Classification of Hydraulic Fluids	46
		2.3.1 Typically Used Hydraulic Fluids	46
		2.3.2 Mineral Oils	47
		2.3.3 Fire-Resistant Fluids	47
	2.4	Additives	49
	2.5	Requirements Imposed on the Hydraulic	
		Liquid	49
	2.6	Exercises	50
	2.7	Nomenclature	53
		Appendix 2A Transfer Functions	54
		Appendix 2B Laminar Flow in Pipes	55
		**	00
3	Hyd	raulic Transmission Lines	59
	3.1	Introduction	59
	3.2	Hydraulic Tubing	59
	3.3	Hoses	64
	3.4	Pressure and Power Losses	
		in Hydraulic Conduits	68
		3.4.1 Minor Losses	68
		3.4.2 Friction Losses	70
	3.5	Modeling of Hydraulic Transmission Lines	72
	3.6	Exercises	76
	3.7	Nomenclature	77
		Appendix 3A The Laplace Transform	77
		The Direct Laplace Transform	77
		The Inverse Laplace Transform	77
		Properties of the Laplace Transform	77
		Laplace Transform Tables	78
		Appendix 3B Modeling and Simulation of	
		Hydraulic Transmission Lines	79
		The Single-Lump Model	79
		The Two-Lump Model	80
		The Three-Lump Model	81
		The Four-Lump Model	81
		Higher-Order Models	82
		Case Study	82
4	Hvd	raulic Pumps	89
•	4.1	Introduction	89
	4.2	Ideal Pump Analysis	91
	4.3	Real Pump Analysis	94
	4.4	Cavitation in Displacement Pumps	97
	T · T		//

	4.5	Pulsatio	n of Flow of Displacement	
		Pumps		98
	4.6	Classific	ation of Pumps	100
		4.6.1	Bent Axis Axial Piston Pumps	100
		4.6.2	Swash Plate Pumps with	
			Axial Pistons	103
		4.6.3	Swash Plate Pumps with	
			Inclined Pistons	105
		4.6.4	Axial Piston Pumps with Rotating	
			Swash Plate-Wobble Plate	106
		4.6.5	Radial Piston Pumps with Eccentric	
			Cam Ring	106
		4.6.6	Radial Piston Pumps with	
			Eccentric Shafts	108
		4.6.7	Radial Piston Pumps	
			of Crank Type	109
		4.6.8	1	109
		4.6.9	1	114
		4.6.10	1	115
		4.6.11	1	117
			Vane Pumps	117
	4.7		Displacement Pumps	122
			General	122
		4.7.2	Pressure-Compensated	
		. – .	Vane Pumps	123
		4.7.3	Bent Axis Axial Piston Pumps with	
			Power Control	125
	4.8		namic Pumps	128
	4.9	Pump S	ummary	130
	4.10		pecification	134
	4.11		S	134
	4.12	Nomeno	clature	137
5	Hyd	raulic Co	ntrol Valves	139
	5.1	Introduo		139
	5.2	Pressure	e-Control Valves	141
		5.2.1	Direct-Operated Relief Valves	141
		5.2.2	Pilot-Operated Relief Valves	144
		5.2.3	Pressure-Reducing Valves	147
		5.2.4	Sequence Valves	152
		5.2.5	Accumulator Charging Valve	155
	5.3	Direction	nal Control Valves	157
		5.3.1	Introduction	157
		5.3.2	Poppet-Type DCVs	157
		5.3.3	Spool-Type DCVs	158

xii Contents

	5.3.4	Control of the Directional	
		Control Valves	161
	5.3.5	Flow Characteristics	
		of Spool Valves	167
	5.3.6	Pressure and Power Losses in the	
		Spool Valves	169
	5.3.7	Flow Forces Acting on the Spool	170
	5.3.8	Direct-Operated Directional	
		Control Valves	172
	5.3.9	Pilot-Operated Directional	
		Control Valves	173
5.4	Check V	alves	175
	5.4.1	Spring-Loaded Direct-Operated	
		Check Valves	175
	5.4.2	Direct-Operated Check Valves	
		Without Springs	176
	5.4.3	Pilot-Operated Check Valves	
		Without External Drain Ports	176
	5.4.4	Pilot-Operated Check Valves with	
		External Drain Ports	178
	5.4.5	Double Pilot-Operated	
		Check Valves	178
	5.4.6	Mechanically Piloted Pilot-Operated	
		Check Valves	179
5.5	Flow Co	ontrol Valves	179
	5.5.1	Throttle Valves	180
	5.5.2	Sharp-Edged Throttle Valves	180
	5.5.3	Series Pressure-Compensated Flow	
		Control Valves	181
	5.5.4	Parallel Pressure-Compensated Flow	
		Control Valves—Three-Way FCVs	184
	5.5.5	Flow Dividers	185
5.6	Exercise	S	188
5.7		clature	190
		ix 5A Control Valve Pressures and	
	Throttle		191
		Conical Poppet Valves	191
		Cylindrical Poppets with	
		Conical Seats	192
		Spherical Poppet Valves	193
		Circular Throttling Area	196
		Triangular Throttling Area	197
	Append		
	Direct-C	Operated Relief Valve	198

Contents Xiii

		Construction and Operation	
		of the Valve	199
		Mathematical Modeling	199
		Computer Simulation	201
		Static Characteristics	201
		Transient Response	202
		Nomenclature	204
6	Acce	ssories	207
	6.1	Introduction	207
	6.2	Hydraulic Accumulators	208
		6.2.1 Classification and Operation	208
		6.2.2 The Volumetric Capacity	
		of Accumulators	210
		6.2.3 The Construction and Operation	
		of Accumulators	211
		6.2.4 Applications of Hydraulic	
		Accumulators	216
		Energy Storage	216
		Emergency Sources of Energy	219
		Compensation for Large	001
		Flow Demands	221
		Pump Unloading	224
		Reducing the Actuator's Response Time	224
		Maintaining Constant	224
		Pressure	225
		Thermal Compensation	226
		Smoothing of Pressure	
		Pulsations	227
		Load Suspension on Load	
		Transporting Vehicles	231
		Absorption of Hydraulic	
		Shocks	232
		Hydraulic Springs	235
	6.3	Hydraulic Filters	237
	6.4	Hydraulic Pressure Switches	238
		6.4.1 Piston-Type Pressure Switches	238
		6.4.2 Bourdon Tube Pressure Switches	239
		6.4.3 Pressure Gauge Isolators	240
	6.5	Exercises	241
	6.6	Nomenclature	243
		Appendix 6A Smoothing Pressure	0.10
		Pulsations by Accumulators	243

xiv Contents

		Appendix 6B Absorption of Hydraulic	
		Shocks by Accumulators	246
		Nomenclature and Abbreviations	249
7	Hvdı	aulic Actuators	251
	7.1	Introduction	251
	7.2	Hydraulic Cylinders	251
		7.2.1 The Construction of Hydraulic	
		Cylinders	252
		7.2.2 Cylinder Cushioning	253
		7.2.3 Stop Tube	256
		7.2.4 Cylinder Buckling	256
		7.2.5 Hydraulic Cylinder Stroke	
		Calculations	258
		7.2.6 Classifications of Hydraulic	
		Cylinders	258
		7.2.7 Cylinder Mounting	261
		7.2.8 Cylinder Calibers	262
	7.3	Hydraulic Rotary Actuators	264
		7.3.1 Rotary Actuator with Rack and	
		Pinion Drive	264
		7.3.2 Parallel Piston Rotary Actuator	264
		7.3.3 Vane-Type Rotary Actuators	265
	7.4	Hydraulic Motors	265
		7.4.1 Introduction	265
		7.4.2 Bent-Axis Axial Piston Motors	266
		7.4.3 Swash Plate Axial Piston Motors	267
		7.4.4 Vane Motors	268
	7.5	7.4.5 Gear Motors Exercises	269
	7.6	Exercises	269 271
	7.0		2/1
		Appendix 7A Case Studies: Hydraulic Circuits	272
			212
8	Hydı	raulic Servo Actuators	281
	8.1	Construction and Operation	281
	8.2	Applications of Hydraulic Servo Actuators	283
		8.2.1 The Steering Systems of Mobile	
		Equipment	283
		8.2.2 Applications in Machine Tools	284
		8.2.3 Applications in Displacement	
		Pump Controls	285
	8.3	The Mathematical Model of HSA	286
	8.4	The Transfer Function of HSA	289
		8.4.1 Deduction of the HSA Transfer Function,	•
		Based on the Step Response	289

Contents XV

		8.4.2 Deducing the HSA Transfer	
		Function Analytically	289
	8.5	Valve-Controlled Actuators	292
		8.5.1 Flow Characteristics	292
		8.5.2 Power Characteristics	295
	8.6	Exercises	296
	8.7	Nomenclature	297
		Appendix 8A Modeling and Simulation	
		of a Hydraulic Servo Actuator	298
		A Mathematical Model	
		of the HSA	299
		Simulation of the HSA	300
		Nomenclature	303
9	Elect	rohydraulic Servovalve Technology	305
	9.1	Introduction	305
	9.2	Applications of Electrohydraulic Servos	306
	9.3	Electromagnetic Motors	306
	9.4	Servovalves Incorporating Flapper	
		Valve Amplifiers	311
		9.4.1 Single-Stage Servovalves	311
		9.4.2 Two-Stage Electrohydraulic	
		Servovalves	313
	9.5	Servovalves Incorporating Jet	
		Pipe Amplifiers	324
	9.6	Servovalves Incorporating Jet	
	~ -	Deflector Amplifiers	327
	9.7	Jet Pipe Amplifiers Versus Nozzle	00 0
	0.0	Flapper Amplifiers	330
	9.8	Exercises	331
10	Mod	eling and Simulation of Electrohydraulic	
		osystems	333
	10.1	Introduction	333
	10.2	Electromagnetic Torque Motors	333
		10.2.1 Introducing Magnetic Circuits	333
		10.2.2 Magnetic Circuit of an Electromagnetic	
		Torque Motor	336
		10.2.3 Analysis of Torque Motors	337
	10.3	Flapper Valves	340
	10.4	Modeling of an Electrohydraulic	
	10 -	Servo Actuator	342
	10.5	Exercises	347
	10.6	Nomenclature	348
		Appendix 10A Modeling and Simulation	0.40
		of an EHSA	349

xvi Contents

			Numerical Values of the Studied	
			System	350
			Torque Motors	351
			Single-Stage Electrohydraulic	
			Servovalves	352
			Two-Stage Electrohydraulic	00-
			Servovalves	354
			Electrohydraulic Servo	001
			Actuators (EHSAs)	358
		Append	lix 10B Design of P, PI, and	000
		PID Cor	8	361
				501
11	Intro		to Pneumatic Systems	367
	11.1		ction	367
	11.2	Peculiar	ities of Pneumatic Systems	367
		11.2.1	Effects of Air Compressibility	367
		11.2.2	The Effect of Air Density	372
		11.2.3	The Effect of Air Viscosity	372
		11.2.4	Other Peculiarities of Pneumatic	
			Systems	372
	11.3	Advanta	ages and Disadvantages of	
		Pneuma	tic Systems	373
		11.3.1	Basic Advantages of Pneumatic	
			Systems	373
		11.3.2	Basic Disadvantages of Pneumatic	
			Systems	373
	11.4 Basic Elements of Pneumatic Systems		ements of Pneumatic Systems	374
		11.4.1	Basic Pneumatic Circuits	374
		11.4.2	Air Compressors	374
		11.4.3	Pneumatic Reservoirs	378
		11.4.4	Air Filters	378
		11.4.5	Air Lubricators	379
		11.4.6	Pneumatic Control Valves	379
	11.5	Case Stu	Idies: Basic Pneumatic Circuits	385
		11.5.1	Manual Control of a Single-	
			Acting Cylinder	385
		11.5.2	Unidirectional Speed Control	
			of a Single-Acting Cylinder	385
		11.5.3	Bidirectional Speed Control	
			of a Single-Acting Cylinder	385
		11.5.4	OR Control of a Single-Acting	
			Cylinder	386
		11.5.5	AND Control of a Single-Acting	
			Cylinder	387

Contents xvii

11	1.5.6	AND Control of Single-Acting	
		Cylinders; Logic AND Control	387
11	1.5.7	Logic NOT Control	387
11	1.5.8	Logic MEMORY Control	388
11	1.5.9	Bidirectional Speed Control of a	
		Double-Acting Cylinder	388
11.	5.10	Unidirectional and Quick Return	
		Control of a Double-Acting	
		Cylinder	389
11.	5.11	Dual Pressure Control of a Double-	
		Acting Cylinder	391
11.	5.12	Semi-Automatic Control	392
11.	5.13	Fully Automatic Control of a	
		Double-Acting Cylinder	392
11.	5.14	Timed Control of a Double-	
		Acting Cylinder	392
11.	5.15	Basic Positional Control of a	
		Double-Acting Cylinder	392
11.	5.16	Electro-Pneumatic Logic AND	396
11.	5.17	Electro-Pneumatic Logic OR	396
11.	5.18	0	397
11.	5.19	Electro-Pneumatic Logic NOT	398
11.6 Ex	ercise	2S	398
11.7 Nomenclature			399
References			
Index			

This page intentionally left blank

Preface

This book examines the construction, principles of operation, and calculation of hydraulic power systems. Special attention is paid to building a solid theoretical background in the subject, which should enable the reader to go on to further study and analysis of the static and dynamic performance of the different fluid power elements and systems. In addition to theory, the book includes case studies of typical construction elements of hydraulic power systems. These elements are categorized, and the special features of their design and performance are discussed.

Following are the chapters in this book:

- Chapter 1, Introduction to Hydraulic Power Systems
- Chapter 2, Hydraulic Oils and Theoretical Background
- Chapter 3, Hydraulic Transmission Lines
- Chapter 4, Hydraulic Pumps
- Chapter 5, Hydraulic Control Valves
- Chapter 6, Accessories
- Chapter 7, Hydraulic Actuators
- Chapter 8, Hydraulic Servo Actuators
- Chapter 9, Electrohydraulic Servovalve Technology
- Chapter 10, Modeling and Simulation of Electrohydraulic Servosystems
- Chapter 11, Introduction to Pneumatic Systems

I am indebted to my colleagues Prof. Dr. Ibrahim Saleh and Prof. Dr. Saad Kassem for the continuous, fruitful, and stimulating discussions we had, and for their objective comments on the book as a whole.

I would also like to express my gratitude to Bosch Rexroth AG, Norgren Ltd., Moog Inc., Famic Technologies Inc., and Olaer Group Ltd. for their kind support and permission to use their illustrations in this book.

Finally, I would like to extend my appreciation and gratitude to the staff of McGraw-Hill Professional, especially Taisuke Soda, senior editor; Stephen M. Smith, editing manager; Pamela A. Pelton, senior production

XX Preface

supervisor; and Jeff Weeks, senior art director. I would also like to thank Arushi Chawla, project manager, and her team at International Typesetting and Composition; Michael McGee for copy editing; Broccoli Information Management for creating the index; Constance Blazewicz for proofreading; and RR Donnelley for printing and binding.

M. Galal Rabie, Ph.D.

Fluid Power Engineering This page intentionally left blank

CHAPTER Introduction to Hydraulic Power Systems

1.1 Introduction

God created the first and most wonderful hydraulic system. It includes a double pump delivering a fluid flow rate of about 10 L/min at 0.16 bar maximum pressure. This pump feeds a piping network stretching more than 100,000 km. That's nearly two and a half times around the Earth. It operates continuously for a very long time, mostly maintenance free. It is the human blood circulatory system. By the age of 50 years, the hearts of 10 men should have pumped a volume of blood equaling that of the great Egyptian pyramid (2,600,000 m³).

As for the hydraulic power systems developed by man, their history started practically 350 years ago. In 1647, Blaise Pascal published the fundamental law of hydrostatics: "Pressure in a fluid at rest is transmitted in all directions." In 1738, Bernoulli published his book *Hydrodynamica*, which included his kinetic-molecular theory of gases, the principle of jet propulsion, and the law of the conservation of energy. By the middle of the nineteenth century, fluid power started playing an important role in both the industrial and civil fields. In England, for example, many cities had central industrial hydraulic distribution networks, supplied by pumps driven by steam engines.

Before the universal adoption of electricity, hydraulic power was a sizable competitor to other energy sources in London. The London Hydraulic Power Company generated hydraulic power for everything from dock cranes and bridges to lifts in private households in Kensington and Mayfair. In the 1930s, during the glory days of hydraulic power, a 12 m³/min average flow rate of water was pumped beneath the streets of London, raising and lowering almost anything that needed to be moved up and down. As a power source,

2 Chapter One

hydraulic power was cheap, efficient, and easily transmitted through 300 km of underground cast-iron piping.

However, as electricity became cheaper and electronically powered equipment grew increasingly sophisticated, so industry and private citizens began to abandon hydraulic power.

High-pressure fluid power systems were put into practical application in 1925, when Harry Vickers developed the balanced vane pump. Today, fluid power systems dominate most of the engineering fields, partially or totally.

1.2 The Classification of Power Systems

Power systems are used to transmit and control power. This function is illustrated by Fig. 1.1. The following are the basic parts of a power system.

- Source of energy, delivering mechanical power of rotary motion. Electric motors and internal combustion engines (ICE) are the most commonly used power sources. For special applications, steam turbines, gas turbines, or hydraulic turbines are used.
- 2. Energy transmission, transformation, and control elements.
- 3. Load requiring mechanical power of either rotary or linear motion.

In engineering applications, there exist different types of power systems: mechanical, electrical, and fluid. Figure 1.2 shows the classification of power systems.

1.2.1 Mechanical Power Systems

The mechanical power systems use mechanical elements to transmit and control the mechanical power. The drive train of a small car is a typical example of a mechanical power system (see Fig. 1.3). The gearbox (3) is connected to the engine (1) through the clutch (2). The input

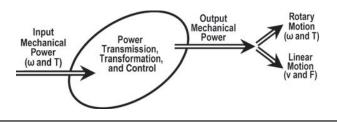


FIGURE 1.1 The function of a power system.

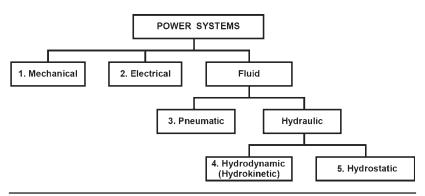


FIGURE 1.2 The classification of power systems.

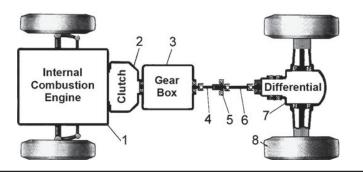


FIGURE 1.3 An automotive drive train.

shaft of the gear box turns at the same speed as the engine. Its output shaft (4) turns at different speeds, depending on the selected gear transmission ratio. The power is then transmitted to the wheels (8) through the universal joints (5), drive shaft (6), and differential (7).

When compared with other power systems, mechanical power systems have advantages such as relatively simple construction, maintenance, and operation, as well as low cost. However, their power-toweight ratio is minimal, the power transmission distance is too limited, and the flexibility and controllability are poor.

1.2.2 Electrical Power Systems

Electrical power systems solve the problems of power transmission distance and flexibility, and improve controllability. Figure 1.4 illustrates the principal of operation of electrical power systems. These systems offer advantages such as high flexibility and a very long power transmission distance, but they produce mainly rotary motion. Rectilinear motion, of high power, can be obtained by converting the rotary motion into rectilinear motion by using a suitable gear system

4 Chapter One

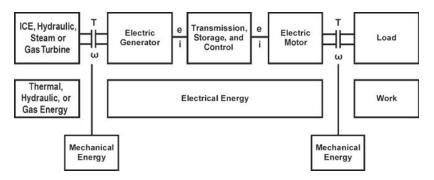


FIGURE 1.4 Power transmission in an electrical power system.

or by using a drum and wire. However, holding the load position requires a special braking system.

1.2.3 Pneumatic Power Systems

Pneumatic systems are power systems using compressed air as a working medium for the power transmission. Their principle of operation is similar to that of electric power systems. The air compressor converts the mechanical energy of the prime mover into mainly pressure energy of compressed air. This transformation facilitates the transmission and control of power. An air preparation process is needed to prepare the compressed air for use. The air preparation includes filtration, drying, and the adding of lubricating oil mist. The compressed air is stored in the compressed air reservoirs and transmitted through rigid and/or flexible lines. The pneumatic power is controlled by means of a set of pressure, flow, and directional control valves. Then, it is converted to the required mechanical power by means of pneumatic cylinders and motors (expanders). Figure 1.5 illustrates the process of power transmission in pneumatic systems.

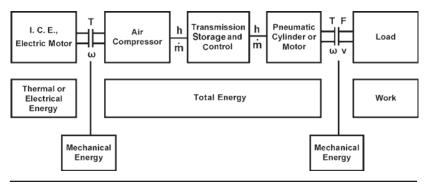


FIGURE 1.5 Power transmission in a pneumatic power system.

1.2.4 Hydrodynamic Power Systems

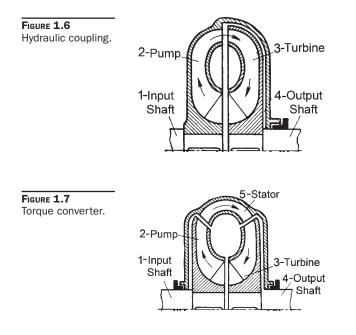
The hydraulic power systems transmit mechanical power by increasing the energy of hydraulic liquids. Two types of hydraulic power systems are used: hydrodynamic and hydrostatic.

Hydrodynamic (also called hydrokinetic) power systems transmit power by increasing mainly the kinetic energy of liquid. Generally, these systems include a rotodynamic pump, a turbine, and additional control elements. The applications of hydrodynamic power systems are limited to rotary motion. These systems replace the classical mechanical transmission in the power stations and vehicles due to their high power-toweight ratio and better controllability.

There are two main types of hydrodynamic power systems: hydraulic coupling and torque converter.

A hydraulic coupling (see Fig. 1.6) is essentially a fluid-based clutch. It consists of a pump (2), driven by the input shaft (1), and a turbine (3), coupled to the output shaft (4). When the pump impeller rotates, the oil flows to the turbine at high speed. The oil then impacts the turbine blades, where it loses most of the kinetic energy it gained from the pump. The oil re-circulates in a closed path inside the coupling and the power is transmitted from the input shaft to the output shaft. The input torque is practically equal to the output torque.

The torque converter is a hydraulic coupling with one extra component: the stator, also called the reactor (5). (See Fig. 1.7.) The stator consists of a series of guide blades attached to the housing. The torque



6 Chapter One

converters are used where it is necessary to control the output torque and develop a transmission ratio, other than unity, keeping acceptable transmission efficiency.

1.2.5 Hydrostatic Power Systems

In the hydrostatic power systems, the power is transmitted by increasing mainly the pressure energy of liquid. These systems are widely used in industry, mobile equipment, aircrafts, ship control, and others. This text deals with the hydrostatic power systems, which are commonly called *hydraulic power systems*. Figure 1.8 shows the operation principle of such systems.

The concepts of hydraulic energy, power, and power transformation are simply explained in the following: Consider a forklift that lifts a load vertically for a distance *y* during a time period Δt (see Fig. 1.9). To fulfill this function, the forklift acts on the load by a vertical force *F*. If the friction is negligible, then in the steady state,

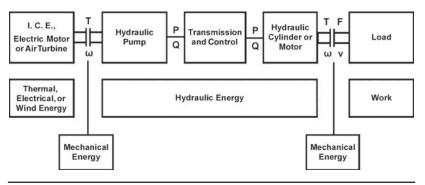


FIGURE **1.8** Power transmission in a hydraulic power system.

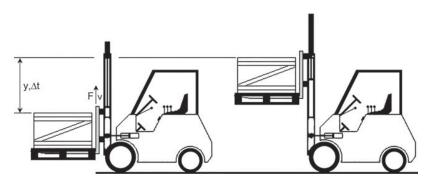


FIGURE 1.9 Load lifting by a forklift.

Introduction to Hydraulic Power Systems 7

this force equals the total weight of the displaced parts (F = mg). The work done by the forklift is

$$W = F y \tag{1.1}$$

By the end of the time period, Δt , the potential energy of the lifted body is increased by *E*, where

$$E = mgy = Fy \tag{1.2}$$

where E = Gained potential energy, J

F = Vertically applied force, N g = Coefficient of gravitational force, m/s²

m = Mass of lifted body, kg

W = Work, J

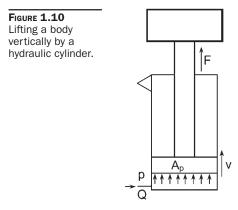
y = Vertical displacement, m

This amount of energy (*E*) is gained during time period Δt . The energy delivered to the lifted body per unit of time is the delivered power *N*, where

$$N = Fy/\Delta t = Fv \tag{1.3}$$

where N = Mechanical power delivered to the load, W v = Lifting speed, m/s

The load is lifted by a hydraulic cylinder. This cylinder acts on the lifted body by a force *F* and drives it with a speed *v*. Figure 1.10 illustrates the action of the hydraulic cylinder. It is a single acting cylinder which extends by the pressure force and retracts by the body weight. The pressurized oil flows to the hydraulic cylinder at a flow rate *Q* (volumetric flow rate, m^3/s) and its pressure is *p*. Neglecting the friction in the cylinder, the pressure force which drives the piston in the extension direction is given by $F = pA_n$.



8 Chapter One

During the time period, Δt , the piston travels vertically a distance *y*. The volume of oil that entered the cylinder during this period is $V = A_p y$. Then, the oil flow rate that entered the cylinder is

$$Q = \frac{V}{\Delta t} = \frac{A_p y}{\Delta t} = A_p v \tag{1.4}$$

Assuming an ideal cylinder, then the hydraulic power inlet to the cylinder is

$$N = Fv = pA_v Q/A_v = Qp \tag{1.5}$$

where A_n = Piston area, m²

p' = Pressure of inlet oil, Pa

 $Q = Flow rate, m^3/s$

V = Piston swept volume, m³

The mechanical power delivered to the load equals the hydraulic power delivered to the cylinder. This equality is due to the assumption of zero internal leakage and zero friction forces in the cylinder. The assumption of zero internal leakage is practical, for normal conditions. However, for aged seals, there may be non-negligible internal leakage. A part of the inlet flow leaks and the speed v becomes less than (Q/A_p) . Also, a part of the pressure force overcomes the friction forces. Thus, the mechanical power output from the hydraulic cylinder is actually less than the input hydraulic power (Fv < Qp).

1.3 Basic Hydraulic Power Systems

Figure 1.11 shows the circuit of a simple hydraulic system, drawn in both functional-sectional schemes and standard hydraulic symbols. The function of this system is summarized in the following:

- The prime mover supplies the system with the required mechanical power. The pump converts the input mechanical power to hydraulic power.
- 2. The energy-carrying liquid is transmitted through the hydraulic transmission lines: pipes and hoses. The hydraulic power is controlled by means of valves of different types. This circuit includes three different types of valves: a pressure control valve, a directional control valve, and a flow control (throttlecheck) valve.
- 3. The controlled hydraulic power is communicated to the hydraulic cylinder, which converts it to the required mechanical power. Generally, the hydraulic power systems provide both rotary and linear motions.

Introduction to Hydraulic Power Systems 9

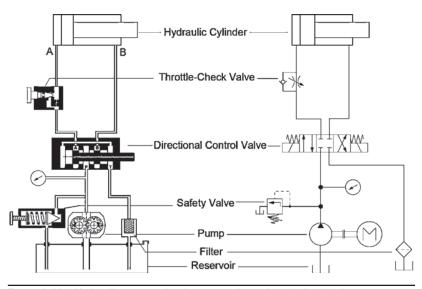


FIGURE 1.11 Hydraulic system circuit, schematic, and symbolic drawings.

1.4 The Advantages and Disadvantages of Hydraulic Systems

The main advantages of the hydraulic power systems are the following:

- 1. High power-to-weight ratio.
- 2. Self-lubrication.
- 3. There is no saturation phenomenon in the hydraulic systems compared with saturation in electric machines. The maximum torque of an electric motor is proportional to the electric current, but it is limited by the magnetic saturation.
- 4. High force-to-mass and torque-to-inertia ratios, which result in high acceleration capability and a rapid response of the hydraulic motors.
- 5. High stiffness of the hydraulic cylinders, which allows stopping loads at any intermediate position.
- 6. Simple protection against overloading.
- 7. Possibility of energy storage in hydraulic accumulators.
- 8. Flexibility of transmission compared with mechanical systems.
- 9. Availability of both rotary and rectilinear motions.
- 10. Safe regarding explosion hazards.

Hydraulic power systems have the following disadvantages:

1. Hydraulic power is not readily available, unlike electrical. Hydraulic generators are therefore required.

10 Chapter One

- 2. High cost of production due to the requirements of small clearances and high precision production process.
- 3. High inertia of transmission lines, which increases their response time.
- 4. Limitation of the maximum and minimum operating temperature.
- 5. Fire hazard when using mineral oils.
- 6. Oil filtration problems.

1.5 Comparing Power Systems

Table 1.1 shows a brief comparison of the different power systems, while Table 1.2 gives the power variables in mechanical, electrical, and hydraulic systems.

System Property	Mechanical	Electrical	Pneumatic	Hydraulic
Input energy source	ICE and electric motor	ICE and hydraulic, air or steam turbines	ICE, electric motor, and pressure tank	ICE, electric motor, and air turbine
Energy transfer element	Mechanical parts, levers, shafts, gears	Electrical cables and magnetic field	Pipes and hoses	Pipes and hoses
Energy carrier	Rigid and elastic objects	Flow of electrons	Air	Hydraulic liquids
Power-to- weight ratio	Poor	Fair	Best	Best
Torque/inertia	Poor	Fair	Good	Best
Stiffness	Good	Poor	Fair	Best
Response speed	Fair	Best	Fair	Good
Dirt sensitivity	Best	Best	Fair	Fair
Relative cost	Best	Best	Good	Fair
Control	Fair	Best	Good	Good
Motion type	Mainly rotary	Mainly rotary	Linear or rotary	Linear or rotary

TABLE 1.1
 Comparison of Power Systems

	Effort		Flow		Power	
	Variable	Units	Variable	Units	Variable	Units
Mech. Linear	Force, F	N	Velocity, v	m/s	N = Fv	W
Mech. Rotary	Torque, T	Nm	Angular speed, ω	rad/s	$N = \omega T$	W
Electrical (DC)	Electric potential, <i>e</i>	V	Electric current, <i>i</i>	A	N = ei	W
Hydraulic	Pressure, P	Ра	Flow rate, Q	m³/s	N = PQ	W

Introduction to Hydraulic Power Systems 11

 TABLE 1.2
 Effort, Flow, and Power Variables of Different Power Systems

1.6 Exercises

1. State the function of the power systems.

2. Discuss briefly the principle of operation of the different power systems giving the necessary schemes.

3. Draw the circuit of a simple hydraulic system, in standard symbols, and explain briefly the function of its basic elements.

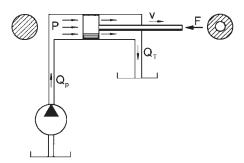
4. State the advantages and disadvantages of hydraulic power systems.

5. Draw the circuit of a simple hydraulic system, including a pump, directional control valves, hydraulic cylinder, relief valve, and pressure gauge. State the function of the individual elements and discuss in detail the power transmission and transformation in the hydraulic power systems.

6. The given figure shows the extension mode of a hydraulic cylinder. Neglecting the losses in the transmission lines and control valves, calculate the loading force, *F*, returned flow rate, $Q_{T'}$ piston speed, *v*, cylinder output mechanical power, $N_{m'}$ and pump output hydraulic power, $N_{h'}$. Comment on the calculation results, given

Delivery line pressure P = 200 bar

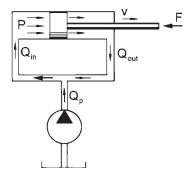
Pump flow rate $Q_p = 40 \text{ L/min}$



12 Chapter One

Piston diameter D = 100 mm Piston rod diameter d = 70 mm

7. The given figure shows the extension mode of a hydraulic cylinder, in differential connection. The losses in the transmission lines and control valves were neglected. Calculate the loading force, *F*, inlet flow rate, Q_{in} , returned flow rate, $Q_{out'}$ piston speed, *v*, cylinder output mechanical power, $N_{m'}$ and pump output hydraulic power, $N_{h'}$. Comment on the calculation results compared with the case of problem 6, given



Delivery line pressure P = 200 bar

Pump flow rate $Q_p = 40 \text{ L/min}$

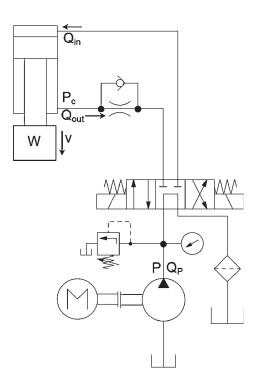
Piston diameter D = 100 mm

Piston rod diameter d = 70 mm

8. Shown is the hydraulic circuit of a load-lifting hydraulic system. The lowering speed is controlled by means of a throttle-check valve. Discuss the construction and operation of this system. Redraw the hydraulic circuit in the load-lowering mode, then calculate the pressure in the cylinder rod side, $P_{C'}$ the inlet flow rate, $Q_{in'}$ outlet flow rate, $Q_{out'}$ pump flow rate, $Q_{p'}$ pump output power, $N_{h'}$ and the area of the throttle valve, A_i . Neglect the hydraulic losses in the system elements, except the throttle valve.

The flow rate through the throttling element is given by: $Q = C_d A_t \sqrt{2\Delta P/\rho}$, where

C_d = Discharge coefficient
ΔP = Pressure difference, Pa
Piston speed = 0.07 m/s
Piston rod side area $A_r = 40 \text{ cm}^2$
Discharge coefficient = 0.611
Weight of the body = 30 kN



9. Redraw the circuit of problem 8 in lifting mode. For the same pump flow rate, safety valve setting, and dimensions, calculate the maximum load that the system can lift. Calculate all of the system operating parameters at this mode. Neglect the hydraulic losses in the system elements, except for the throttle valve.

1.7 **Nomenclature**

- A_p = Piston area, m² E = Gained potential energy, J
- F = Vertically applied force, N
- $g = \text{Coefficient of gravitational force, m/s}^2$
- m = Mass of lifted body, kg
- N = Mechanical power delivered to the load, W
- p = Pressure, Pa
- $Q = \text{Flow rate, } \text{m}^3/\text{s}$
- v = Lifting speed, m/s
- $V = Piston swept volume, m^3$
- W = Work, J
- y = Vertical displacement, m

References

- 2007 M. G. Rabie, "On the Application of Oleo-Pneumatic Accumulators for the Protection of Hydraulic Transmission Lines Against Water Hammer—A Theoretical Study," *Int. J. Fluid Power*, Vol. 8, No. 1, 2007, pp. 39–49.
- Study," Int. J. Fluid Power, Vol. 8, No. 1, 2007, pp. 39–49.
 2007 M. Metwally, I. Saleh, M. G. Rabie, and N. Girgis, "Effects of Air and Fuel Flow on the Dynamic Performance of a Turboshaft Gas Turbine Engine, Part I: Modeling and Simulation," Proceedings of the 12th ASAT Conference, MTC, Cairo, Egypt, May 29–31, 2007, Paper TM1-01.
- 2007 M. Metwally, I. Saleh, M. G. Rabie, and N. Girgis, "Effects of Air and Fuel Flow on the Dynamic Performance of a Turboshaft Gas Turbine Engine, Part II: Analysis of the Engine Dynamic Performance," *Proceedings of the 12th ASAT Conference*, MTC, Cairo, Egypt, May 29–31, 2007, Paper TM1-02.
 2006 S. Z. Kassab, I. G. Adam, M. A. Swidan, and M. G. Rabie, "Influence of
- 2006 S. Z. Kassab, I. G. Adam, M. A. Swidan, and M. G. Rabie, "Influence of Operating and Construction Parameters on the Behavior of Hydraulic Cylinder Subjected to Jerky Motion," *Proceedings of the 8th International Conference of Fluid Dynamics & Propulsion*, Sharm El-Sheikh, Sinai, Egypt, Dec. 14–17, 2006, pp. 1–8. Copyright © 2006 by ASME.
- 2006 T. A. Saleh, M. G. Rabie, and S. E. Abdou, "Investigation of Static and Dynamic Performance of Pressure Compensated Variable Displacement Swash Plate Axial Piston Pump," *Proceedings of the 12th AMME Conference*, MTC, Cairo, Egypt, May 16–18, 2006, pp. 315–333.
- 2006 M. Metwally, M. G. Rabie, N. Girgis, and I. Saleh, "Dynamic Performance of an Electrohydraulic Servo Actuator with Contactless Controlled Spool," *Proceedings* of the 12th AMME Conference, MTC, Cairo, Egypt, May 16–18, 2006, pp. 467–489.
- 2005 Z. A. Ibrahim, M. I. A. Elsherif, M. G. Rabie, and S. A. Hegazy, "Design and Analysis of the Dynamic Performance of a Vehicle Active Suspension System," *Proceedings of the 11th ASAT Conference*, MTC, Cairo, Egypt, May 17–19, 2005, Paper FH-03, pp. 147–163.
- Z. A. Ibrahim, M. G. Rabie, S. A. Hegazy, and I. A. Elsherif, "Experimental and Theoretical Investigation of Dynamic Behavior of Oleo-Pneumatic Car Suspension," *Proceedings of the 11th ASAT Conference*, MTC, Cairo, Egypt, May 17–19, 2005, Paper FH-04, pp. 131–146.
 Z. X. Kassab, M. A. Swidan, I. G. Adam, and M. G. Rabie, "Dynamic Behavior
- 2004 S. Z. Kassab, M. A. Swidan, I. G. Adam, and M. G. Rabie, "Dynamic Behavior of Hydraulic Cylinder Subjected to Jerky Motion During Load Lowering, Part 1: Experimental Work," *Proceedings of the 11th AMME Conference*, MTC, Cairo, Egypt, Nov. 23–25, 2004, Paper DV-01, pp. 38–52.
- 2004 S. Z. Kassab, M. A. Swidan, I. G. Adam, and M. G. Rabie, "Dynamic Behavior of Hydraulic Cylinder Subjected to Jerky Motion During Load Lowering, Part 2: Modeling and Simulation," *Proceedings of the 11th AMME Conference*, MTC, Cairo, Egypt, Nov. 23–25, 2004, Paper DV-02, pp. 53–72.
- 2003 A. Esposito, *Fluid Power with Applications*, 6th ed., Prentice Hall, Upper Saddle River, N.I., 2003.
- 2003 A. A. El-Sayed, M. H. Gobran, M. G. Rabie, and M. R. Shalaan, "Investigation of Characteristics of an Electrohydraulic Servoactuator Incorporating Jet Pipe Amplifier," *Proceedings of the 10th ASAT Conference*, MTC, Cairo, Egypt, May 13–15, 2003, Paper HF-03, pp. 109–123.

- 2003 Z. A. Ibrahim, S. A. Hegazy, I. A. Elsherif, and M. G. Rabie, "Dynamic Behavior of Gas Charged Single Tube Shock Absorber," *Proceedings of the 10th* ASAT Conference, MTC, Cairo, Egypt, May 13–15, 2003, Paper HF-08, pp. 185–201.
- 2002 O. G. El-Sayed, M. G. Rabie, and R. El-Taher, "Prediction and Improvement of Steady-State Performance of a Power Controlled Axial Piston Pump," J. Dyn. Sys. Meas. Control. Vol. 124. Sept. 2002, pp. 443–451.
- Sys. Meas. Control, Vol. 124, Sept. 2002, pp. 443–451.
 2001 Y. Du, A. V. Mamishev, B. C. Lesieutre, M. Zahn, and S. H. Kang, "Moisture Solubility for Differently Conditioned Transfer Oils," *IEEE Transactions on Dielectrics and Electrical Insulation*, Vol. 8, No. 5, Oct. 2001, pp. 805–811.
- 2001 Eaton Corp., Industrial and Mobile Fluid Power, Product Literature 900, Release 1.1, CD from Eaton Corp., Eden Prairie, Minn., 2001.
- 2001 O. G. El-Sayed, M. G. Rabie, and R. El-Taher, "Experimental and Theoretical Study of the Static and Dynamic Behavior of a Variable-Displacement Pump with Power Control," *Modeling, Measurement & Control*, B-2001 (AMSE), Vol. 70, No. 5, pp. 11–30.
- 1999 A.-N. Zayed, Summary for Engineers, Ziad Press, Alexandria, Egypt, 1999.
- 1999 Y. Du, A. V. Mamishev, B. C. Lesicutre, M. Zahn, and S. H. Kang, "Measurement of Moisture Solubility for Differently Conditioned Transfer Oils," *Proceedings of the 13th International Conference on Dielectric Liquids* (ICDL99), Nara, Japan, July 20–25, 1999, pp. 357–360.
- 1999 Mannesmann Rexroth AG, Interactive Hydraulic Designer, CD from Brueninghaus Hydromatic & Rexroth Hydraulics, Lohr am Main, Germany, 1999.
- 1999 Mannesmann Rexroth AG, Product Catalogue of Axial Piston Units, CD from Brueninghaus Hydromatic, Lohr am Main, Germany, 1999.
- 1999 Vickers Incorporated, Electronic Catalogue, Vol. X, CD from Vickers Incorporated, Hampshire, U.K., 1999.
- 1999 M. A. Karkub, O. E. Gad, and M. G. Rabie, "Predicting Axial Piston Pump Performance Using Neural Networks," Int. J. of Mechanism and Machine Theory, Vol. 34, 1999, pp. 1211–1226.
- 1998 R. Bosch GmbH., Electronic Reference Library, Hydraulics, CD from Bosch Automation Technology, Stuttgart, Germany, 1998.
- 1998 P. Hannifin GmbH., Hydraulic Control, Catalogue 2500/GB, CD from Parker Hydraulics, Kaarst, Germany, 1998.
- 1998 Sauer Sunsdstrand Co., All Product Technical, Application, and Service/ Repair Information, CD from Sauer Sunsdstrand Co., Ames, Iowa, 1998.
- 1998 S. Y. Ibrahim, M. G. Rabie, and A. H. Lotfy, "Experimental and Theoretical Investigation of the Performance of the Servoactuator of a Hydraulic Power Steering System," *Proceedings of the 8th AMME Conference*, MTC, Cairo, Egypt, May 1998, pp. 395–407.
- 1997 R. N. Brown, Compressors: Selection and Sizing, Gulf Professional Publishing, Houston, Tex., 1997.
- 1997 M. G. Rabie, "On the Validity of the Lumped Parameter Models for Fluid Flow Between Coaxial Pipes," *Modeling, Measurement & Control*, B-1997 (AMSE), Vol. 63, No. 1, 2, pp. 31–47.
- 1997 M. M. Samir, M. A. Katary, and M. G. Rabie, "Investigation of Helicopter Stability Considering the Effect of Its Hydraulic Servoactuator and Autopilot," *Proceedings of the 7th ASAT Conference*, MTC, Cairo, Egypt, Vol. 1, May 13–15, 1997, Paper FD-1, pp. 63–82.
- 1996 Mannesmann Rexroth AG, Industrial Hydraulic Valve Catalogue and Pump and Motor Catalogue, CD from Rexroth USA, Bethlehem, Pa., 1996.
- 1996 P. K. B. Hodges, Hydraulic Fluids, John Wiley & Sons, Inc., New York, 1996.
- 1996 M. Elsaid, M. G. Rabie, and A. A. Khattab, "Investigation of the Transient Behavior of End Position Cushioning in Hydraulic Cylinders," *Proceedings of the 7th AMME Conference*, MTC, Cairo, Egypt, May 28–31, 1996, Paper PE-1, pp. 351–364.
- 1994 M. G. Rabie, "Improvement of Performance of an Electrohydraulic Servoactuator Performance by Developing a Pseudo Derivative Controller," *Modeling, Measurement & Control*, B-1994 (AMSE), Vol. 54, No. 3, pp. 9–23.

- 1994 M. G. Rabie, M. A. Ali, and Z. A. Ibrahim, "On the Synchronization of Motion of Hydraulic Cylinders by Spool Type Flow Divider," *Proceedings of the 6th AMME Conference*, MTC, Cairo, Egypt, Vol. 1, May 3–5, 1994, Paper PE-6, pp. 545–561.
- 1993 M. G. Rabie and I. Saleh, "On the Effect of Location of Damping Orifice on the Performance of Hydraulic Systems with Counterbalance Valve," *Bulletin of Fac. of Eng.*, Ain Shams Univ., Cairo, Egypt, Vol. 28, No. 1, March 1993, pp. 537–553.
 1993 M. G. Rabie, M. A. Awad, E. I. Imam, and N. A. Gadallah, "Experimental
- 1993 M. G. Rabie, M. A. Awad, E. I. Imam, and N. A. Gadallah, "Experimental and Theoretical Investigation of the Transient Response of Hydraulic Valve Controlled Actuators," *Alex. Eng. J.*, Alex. Univ., Alexandria, Egypt, Vol. 32, No. 1, April 1993, pp. A7–A16.
- 1993 M. G. Rabie, S. M. Metwally, and S. E. Abdou, "Design of a New Controller for a Hydraulic Servomechanism," *Proceedings of the 4th ASAT Conference*, MTC, Cairo, Egypt, Vol. 1, May 4–6, 1993, Paper FM-3, pp. 175–188.
- 1991 M. G. Rabie and Y. Younis, "Investigation of Performance of a Direct Operated Hydraulic Pressure Reducer, Approach by Block Bond Graph," *Alex. Eng. J.*, Alex. Univ., Alexandria, Egypt, Vol. 30, April 1991, pp. 115–120.
- 1991 M. G. Rabie, "On the Dynamics of Fluid Flow Between Two Coaxial Pipes: A Lumped Parameter Model," Eng. Res. Bulletin of Fac. of Eng. & Tech., Mataria, Univ. of Helwan, Cairo, Egypt, Vol. 3, March 1991, pp. 1–11.
- 1991 M. G. Rabie and H. E. Hafez, "Modeling by Block Bond Graph and Investigation of Dynamic Performance of a Hydraulic Pressure Reducer," *Bulletin of Fac. of Eng.*, Ain Shams Univ., Cairo, Egypt, Vol. 26, No. 1, March 1991, pp. 492–509.
- 1991 M. G. Rabie, S. A. Kassem, S. A. El-Sayed, M. A. Aziz, and O. G. El-Sayed, "Static and Dynamic Performance of Pilot Operated Hydraulic Relief Valves," *Proceedings of the 4th ASAT Conference*, MTC, Cairo, Egypt, May 14–16, 1991, Paper FM-1, pp. 135–143.
- 1990 C. R. Burrows and K. A. Edges, *Fluid Power Components and Systems*, RSP, U.K., and John Wiley & Sons, Inc., New York, 1990.
- 1990 R. A. Nasca, Testing Fluid Power Components, Industrial Press, New York, 1990.
- 1990 F. Yeaple, Fluid Power Design Handbook, 2d ed., M. Dekker, New York, 1990.
- 1990 M. G. Rabie and I. Saleh, "On the Dynamics of Pressure Compensated Variable Geometric Volume Axial Piston Pump," *Eng. Res. Bulletin of Fac. of Eng. & Tech.*, Mataria, Univ. of Helwan, Cairo, Egypt, Vol. 6, Dec. 1990, pp. 50–60.
- 1990 M. G. Rabie and U. M. Ibrahim, "Modeling and Simulation of a Compact Electrohydraulic Servoactuator," *J. Fac. of Eng.*, Cairo Univ., Cairo, Egypt, Vol. 37, No. 4, Dec. 1990, pp. 1003–1018.
- 1989 M. J. Pinches and J. G. Ashby, *Power Hydraulics*, Prentice Hall International, London, 1989.
- 1989 J. Watton, Fluid Power Systems: Modeling, Simulation, Analogue and Microprocessor Control, Prentice Hall, Hertfordshire, U.K., 1989.
- 1989 M. G. Rabie, S. A. Kassem, S. A. El-Sayed, M. A. Aziz, and O. G. El-Sayed, "Block Bond Graph and TUTSIM: A Powerful Tool for Nonlinear Dynamic System Modeling and Simulation," *Alex. Eng. J.*, Alex. Univ., Alexandria, Egypt, Vol. 28, No. 3, July 1989, pp. 519–537.
- Vol. 28, No. 3, July 1989, pp. 519–537.
 1989 M. G. Rabie, "Simulation and Analysis of a Pilot-Operated Hydraulic Pressure Reducer," *Proceedings of the 3rd ASAT Conference*, MTC, Cairo, Egypt, Vol. 4, April 4–6, 1989, Paper FD-5, pp. 371–381.
- 1988 S. A. Kassem, M. G. Rabie, E. S. El-Adawy, Y. I. Younis, and H. Ahmed, "Dynamic Analysis of Hydraulic Transmission Lines by a Lumped Model," *Bulletin of Fac. of Eng.*, Ain Shams Univ., Cairo, Egypt, Vol. 22, No. 2, 1988, pp. 1–18.
- 1987 Mannesmann Rexroth AG, Hydraulic Components, General Catalogue, Mannesmann Rexroth AG, Lohr am Main, Germany, 1987.
- 1986 H. Dorr et al., *Proportional and Servo Valve Technology*, Mannesmann Rexroth AG, Lohr am Main, Germany, 1986.
- 1986 M. G. Rabie, "About the Lumped Parameter Approach to Hydraulic Line Modeling," *Proceedings of the 2nd AMME Conference*, MTC, Cairo, Egypt, Vol. 1, May 6–8, 1986, Paper DYN-4, pp. 31–46.

1985 E. W. Reed and I. S. Larman, *Fluid Power with Microprocessor Control*, Prentice Hall, 1985.

1985 M. J. Tonyan, Electronically Controlled Proportional Valves, M. Dekker, New York, 1985.

- 1984 W. Gotz, *Hydraulics: Theory and Applications from Bosch*, Robert Bosch GmbH. Hydraulics Division, Stuttgart, Germany, 1984.
- 1984 A. Henn, Fluid Power Trouble Shooting, M. Dekker, New York, 1984.
- 1984 J. Pippinger, Hydraulic Valves and Controls, M. Dekker, New York, 1984.
- 1984 S. A. Kassem and M. G. Rabie, "Bond Graph and Investigation of Dynamics of a Class of Hydraulic Flow Control Valves," *Proceedings of the 1st AMME Conference*, MTC, Cairo, Egypt, Vol. 1, May 29–31, 1984, Paper DYN-12, pp. 121–130.
- 1983 R. P. Lambeck, *Hydraulic Pumps and Motors*, M. Dekker, New York, 1983.
- 1982 J. A. Sullivan, Fluid Power: Theory and Applications, 2d ed., Reston, Va., 1982.
- 1982 M. G. Rabie and M. Lebrun, "Modeling by Bond Graph and Simulation of an Electrohydraulic Servomotor," *Proceedings of 2nd MDP Conference of Cairo University*, Supplementry Volume, Dec. 27–29, 1982, pp. 45–54.
- M. G. Rabie and M. Lebrun, "Modeling by Bond Graph and Simulation of a Bi-axial Electrohydraulic Fatigue Machine," *IASTED Symp. Modeling, Ident., Cont.,* Davos, Switzerland, Feb. 18–21, 1981 (in French).
 M. G. Rabie and M. Lebrun, "Modeling by Bond Graph and Simulation of an
- 1981 M. G. Rabie and M. Lebrun, "Modeling by Bond Graph and Simulation of an Electrohydraulic Servovalve of Two Stages," *RAIRO Automatic Systems Analysis* and Control, Vol. 15, No. 2, 1981, pp. 97–129 (in French).
- 1980 D. McCloy and H. R. Martin, The Control of Fluid Power: Analysis and Design, 2d ed., Ellis Haward, West Sussex, U.K., 1980.
- 1979 A. Baz, M. G. Rabie, H. Zaki, and A. Barakat, "Hydraulic Servo with Built-in Tuned Damper," *Fluidic Quarterly*, Vol. 11, No. 2, June 1979, pp. 1–24.
- 1978 A. Baz, A. Barakat, and M. G. Rabie, "Leakage in Hydraulic Spool Valves," Proceedings of National Conference on Fluid Power, 32d annual meeting, Philadelphia, Nov. 7–9, 1978, pp. 37–44.
- 1978 A. Baz, M. G. Rabie, and H. Zaki, "A New Class of Spool Valves with Built-in Dampers," paper presented at the Design Engineering Conference Show of ASME, Chicago, April 17–20, 1978.
- 1977 S. A. Braillon, *Electro-magnetic Proportional Solenoids as Control Elements of Hydraulic Valves*, MSM Division, France, 1977, pp. 81–89 (in French).
 1977 M. G. Rabie and I. I. Rashed, "Effect of the Internal Leakage in the Cylinder
- 1977 M. G. Rabie and I. I. Rashed, "Effect of the Internal Leakage in the Cylinder on the Static and Dynamic Characteristics of the Hydraulic Booster," *Bulletin of the Fac. of Eng.*, Cairo Univ., Cairo, Egypt, 1976/1977, Paper 1, pp. 1–22.
- 1976 A. B. Goodwin, Fluid Power Systems, Macmillan Press Ltd., London, 1976.
- 1976 J. Lallement, "Study of the Dynamic Behavior of Hydraulic Lines" (in French), Les Memoir Techniques du Centre Technique des Industries Mecaniques, Senlis, France, No. 27, Sept. 1976.
- 1975 D. Karnopp and R. Rosenberg, *System Dynamics: A Unified Approach*, John Wiley & Sons, Inc., New York, 1975.
- 1973 D. McCloy and H. R. Martin, *The Control of Fluid Power*, Longman, London, 1973.
- 1969 B. Nekrasov, *Hydraulics for Aeronautical Engineers*, Mir Publishers, Moscow, 1969.
- 1967 H. E. Merrit, *Hydraulic Control Systems*, John Wiley & Sons, Inc., New York, 1967.
- 1957 H. G. Conway, *Aircraft Hydraulics*, Vol. 1, Chapman and Hall Ltd., London, 1957.
- 1957 H. G. Conway, Aircraft Hydraulics, Vol. 2, Chapman and Hall Ltd., London, 1957.



Laboratory Book



Hydraulic Power Systems

Laboratory Work

Experiment No. 1 Centrifugal Pump Characteristics

Students Name:	
Class:	Nr.:
Date:	

Centrifugal Pump Characteristics

This experiment is designed to measure the flow characteristics of a centrifugal pump; Head (Flow rate). The set-up includes:

- > the control of the pump exit pressure
- > the measurement of the pump exit pressure
- > the calculation of pressure head and
- > the measurement of the pump flow rate.

1. Test stand



Fig.1 Centrifugal pump test stand

The test stand is shown by Fig.1, while its hydraulic circuit is given by Fig.2. The system consists of the following elements:

- (1) Water tank
- (3) Centrifugal pump
- (5) Throttle valve
- (7) Return pipe line
- (9) Orifice meter inlet pressure gauge
- (11) Power indicating lamb
- (13) Motor running indicating lamb

- (2) Pump suction pipe
- (4) Electric motor (n=2800 rpm)
- (6) Orifice flow meter
- (8) pump exit pressure gauge
- (10) Orifice meter outlet pressure gauge
- (12) Motor on/off switch
- (14) Pump suction valve

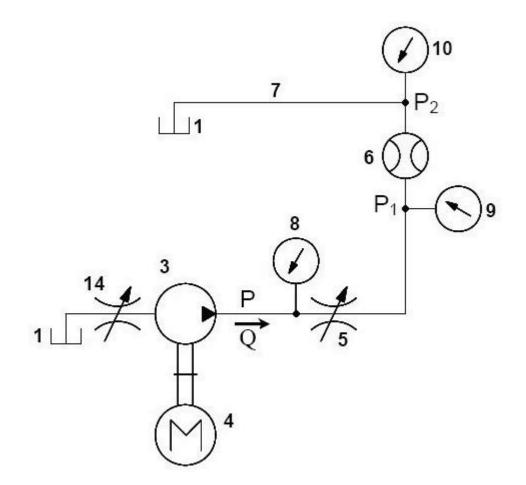


Fig.2 Hydraulic circuit of the centrifugal pump test stand

The pump exit pressure (P) is measured in (bar). The corresponding head is:

H = P/pg

For water H = 10 P (Where P is in bar and H is in meters)

The pump exit pressure is controlled by the throttle valve (5) and measured by the pressure gauge (8).

The pump flow rate is measured by the orifice flow meter (6) and pressure gauges (9&10). The flow rate through the orifice meter is calculated as follows.

$$Q = C_d A_o \sqrt{\frac{2}{\rho}(P_1 - P_2)}$$

Where $Q = Water flow rate, m^3/s$

 A_0 = Orifice area = 78.54 mm²

 ρ = Water Density = 1000 kg/m³

 $P_1 = Orifice meter inlet pressure, Pa$

 $P_2 = Orifice meter outlet Pressure, Pa$

C_d = Discharge coefficient, (= 0.611 for sharp edged orifice)

Or $Q = 68.817 \sqrt{P_1}$

Where Q = Water flow rate, L/min

 $P_1 = Orifice meter inlet pressure, bar$

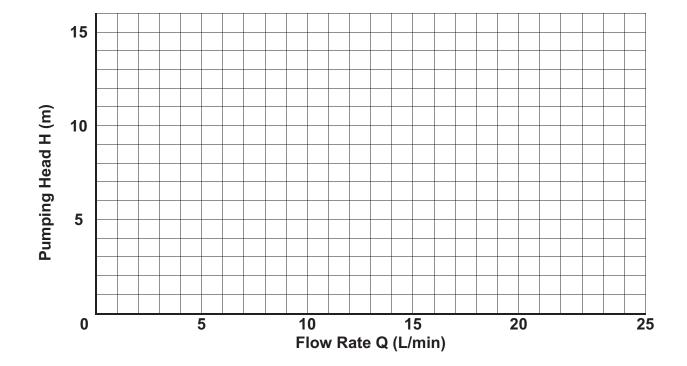
 P_2 = Orifice meter outlet Pressure (= 0 bar for this setup)

2. Steps of measurements

- (1) Close the throttle valve (5) completely.
- (2) Connect the power cable; the power lamb (13) goes on (red color).
- (3) Switch the electric motor on, switch No. (12); the indicating lamb (11) goes on (green color)
- (4) Get the readings of the three pressure gauges, and record them on the given table.
- (5) Open the throttle valve (5) gradually and record the pressure gauges readings until the valve is fully open.
- (6) Close the throttle valve (5) gradually and record the pressure gauges readings until the valve is fully closed.
- (7) Switch the electric motor off, switch No. (12); the indicating lamb (11) goes off.
- (8) Disconnect the power cable; the power lamb (13) goes off.

	Р	P 1	P ₂	Q	Н
No.	bar	hau	bar	$Q = 68.817 \sqrt{P_1}$	H =10 P
	Dai	bar	Dai	L/min	m
1.					
2.					
3.					
4.					
5.					
6.					
7.					
8.					
9.					
10.					
11.					
12.					
13.					
14.					
15.					

3. Results



4. Discussion and conclusion



Modern Academy for Engineering & Technology



Hydraulic Power Systems

Laboratory Work

Experiment No. 2

Hydraulic Training Unit

Students Name:	Nr.:
Date:	

1. Aims:

- a. Recognize the construction of the hydraulic training unit.
- b. Understand the function of its hydraulic circuit.
- c. To be acquainted with the existing hydraulic elements, their function and symbol.
- d. Put the power pack in operation and adjust its relief pressure.

2. HYDRAULIC CIRCUIT OF THE POWER PACK

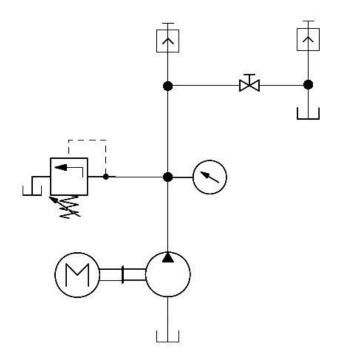


Fig.2.1 Hydraulic circuit of the power pack

Add the elements number, as listed in table 2.1, then explain briefly the function of the circuit.

3. ELEMENTS OF THE HYDRAULIC TRAINING UNIT

Table 2.1 gives the numbering and names of the basic elements of the hydraulic training unit. Connect the numbers to the corresponding element on all of the images.



Fig.2.2 Front view of the hydraulic training unit



Fig.2.3 Front view of the power pack

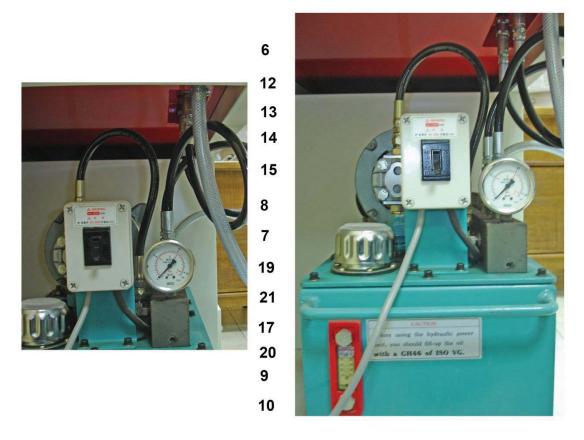


Fig.2.4 Side view of the power pack

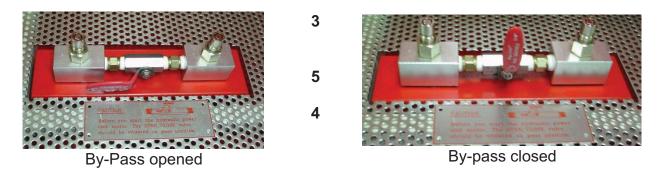


Fig.2.5 By-pass arrangement

Table 2.1	Elomonte	of the	bydraulic	training up	iŧ
			nyuraulic	training un	п

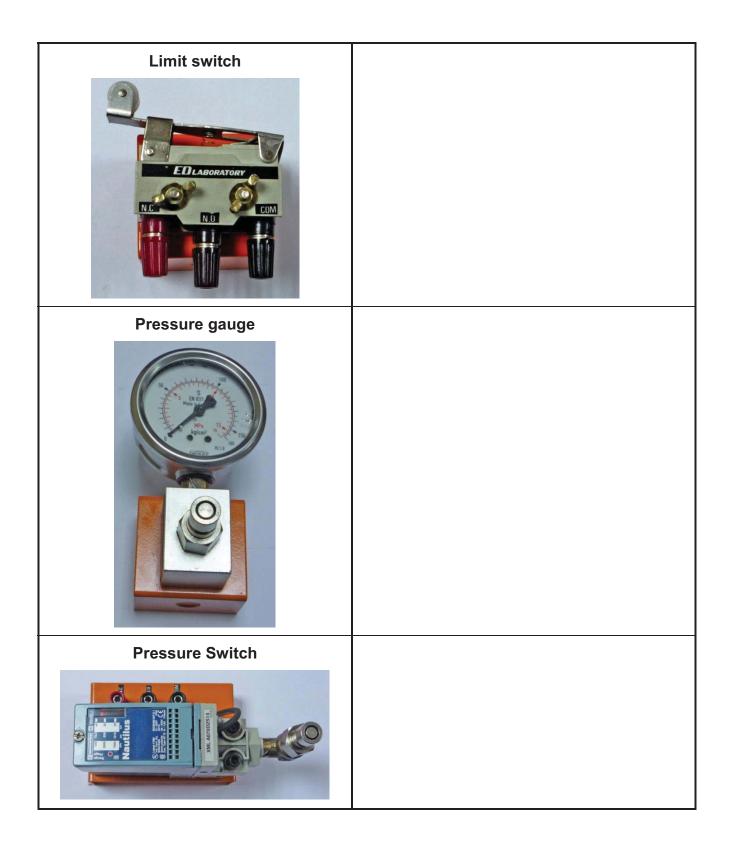
No.	Name
1	Metallic panel for attachment of hydraulic elements
2	Electric control panel
3	Hydraulic pressure line connector
4	Return line connector
5	By-pass valve
6	Oil sump
7	Gear pump
8	Electric motor
9	Hydraulic tank
10	Oil level indicator
11	Pump suction line
12	Pump delivery line
13	High pressure line
14	Return line
15	Oil sump drain line
16	Drain manifold
17	Control block
18	Safety valve
19	Pressure gauge
20	Air breather
21	Main switch

4. AVAILABLE VALVES AND ELEMENTS

In addition to the flexible hoses, the following elements are available. State briefly the function of each of them.

Element	Symbol and Function
Check valve	
5	
Pilot operated check valve	
P-COMPA P-COMP	
Relief valve	

Sequence valve	
Throttle-check valve	
Connectors	
Cylinder	
Transparent cylinder	





4. REGULATIONS OF POWER PACK OPERATION

Before operation:

Operation and relief valve setting:

Comments:



Hydraulic Power Systems

Laboratory Work

Experiment No. 3

Cavitation in Hydraulic Displacement pumps

Students Name:	
Class:	Nr.:
Date:	

1. AIMS

- 1- Understand the cavitation phenomenon
- 2- Define and understand the displacement pump flow characteristics
- 3- Visualize the cavitation phenomenon
- 4- Measure the pump flow characteristics

2. HYDRAULIC SYSTEM OF THE PUMP TEST STAND

2.1 Construction of the hydraulic system

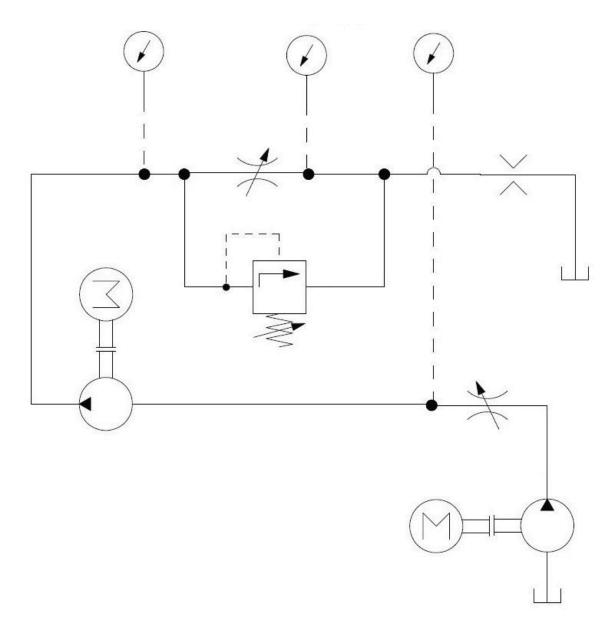


Fig.3.1 Hydraulic circuit of the pump test stand

Add the elements number, as listed in table 2.1, to Fig.3.1, and then explain briefly the construction of system.

Table 3.1 Elements of the pump test stand

No	Part Name
1	Hydraulic Tank(Reservoir)
2	Filling neck with air breather
3	Oil level indicator
4	Booster pump suction line
5	Booster pump
6	Booster pump driving motor
7	Booster pump exit line
8	Throttle valve
9	Hose connecting suction pressure to pressure gauge
10	Transparent pipe
11	Gear pump suction line
12	Gear Pump
13	Gear pump driving motor
14	Gear pump exit line
15	Relief valve
16	Throttle valve
17	Orifice flow meter
18	Pressure gauge (Gear Pump exit pressure)
19	Pressure gauge (Orifice meter inlet pressure)
20	Pressure gauge (Gear Pump inlet pressure)
21	Booster pump electric switch
22	Booster pump operation indicating lamp
23	Gear pump electric switch
24	Gear pump operation indicating lamp

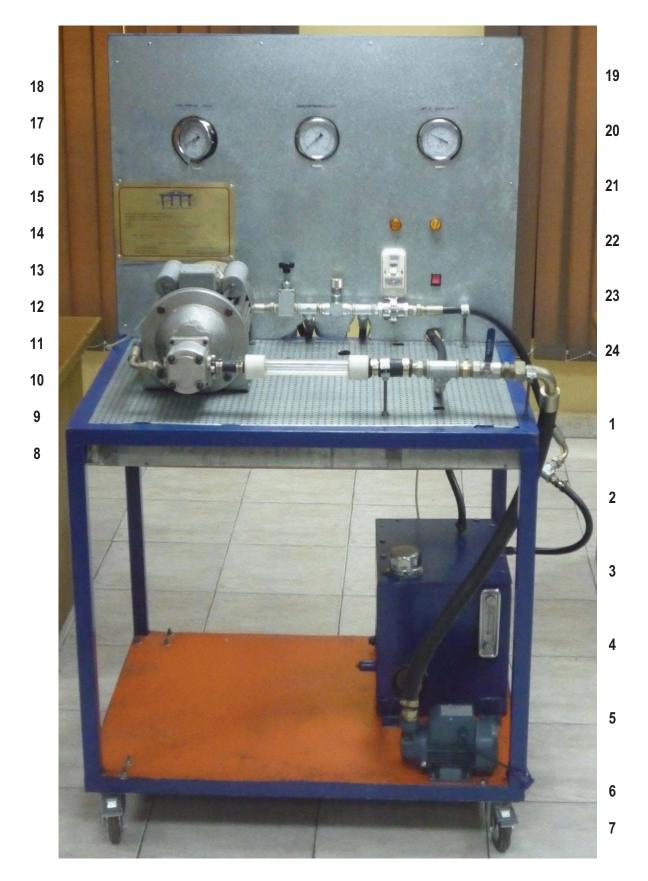


Fig.3.2 Pump test stand































2.2 Operation of the hydraulic system

2.2.1 Gear Pump Inlet Pressure Control

2.2.2 Gear Pump Exit Pressure Control

2.2.3 Gear Pump Flow Rate Measurement



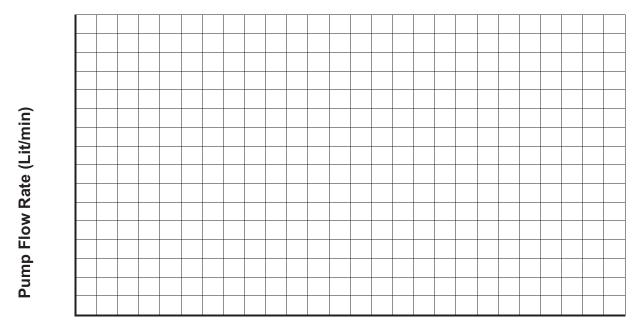
3. MEASUREMENT OF THE PUMP CHARACTERISTICS

Flow Characteristics; Q_P(P_P) at constant inlet pressure

Inlet Pressure = Constant = bar

P _P (bar)	P _{FM} (bar)	Q _P (Lit/min)

P _P (bar)	P _{FM} (bar)	Q _P (Lit/min)



Pump Exit Pressure (bar)



Comments on the Pump Flow Characteristics

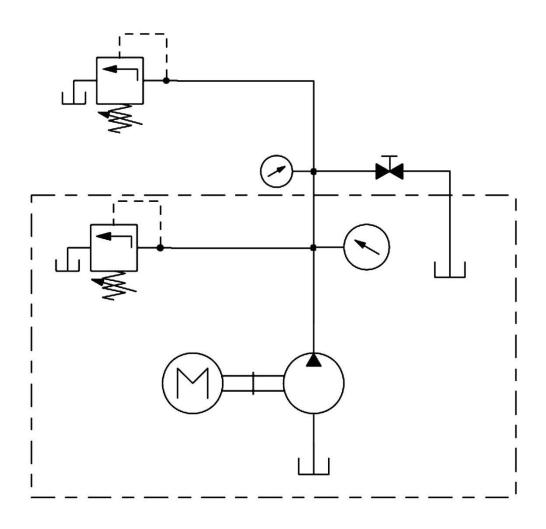


Hydraulic Power Syst

Laboratory Work

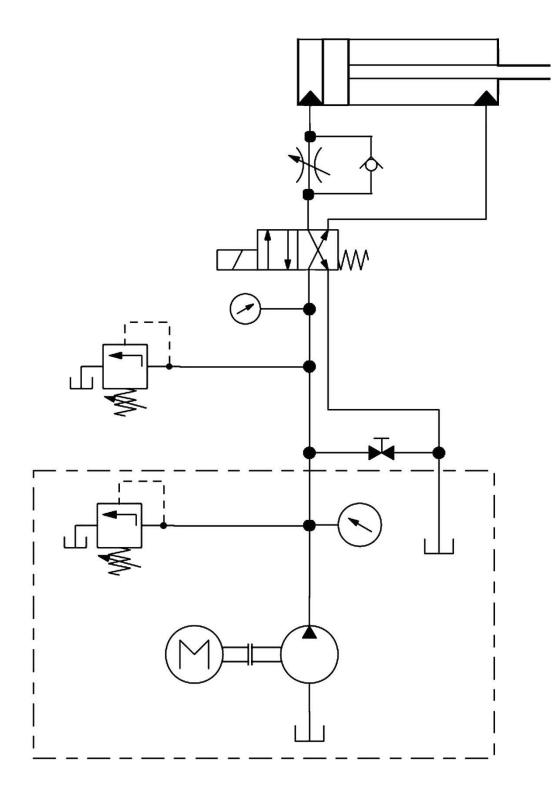
Hydraulic Circuits

Students Name:	
Class:	Nr.:
Date:	



1. Number the elements of the circuit and state the names and function of the circuit parts in the following table

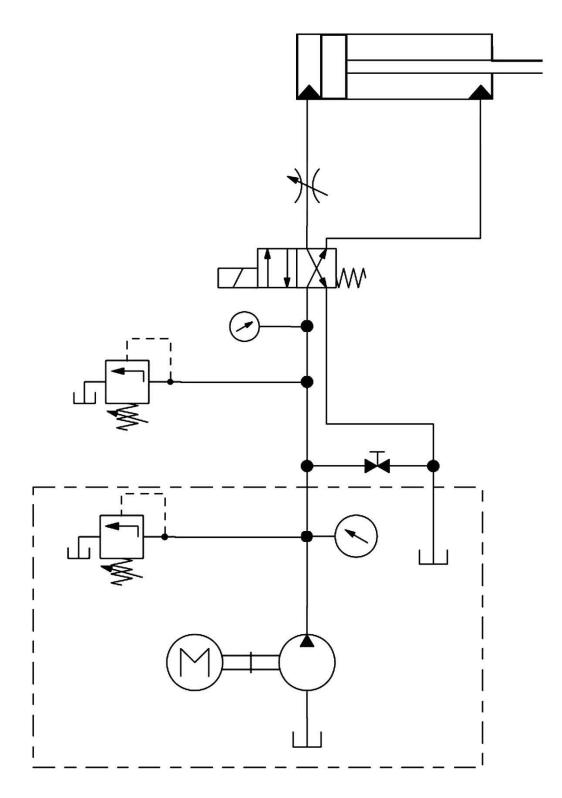
No.	Name	Function
1		
2		
3		
4		
5		
6		
7		
8		
9		
10		
11		
12		
13		
14		





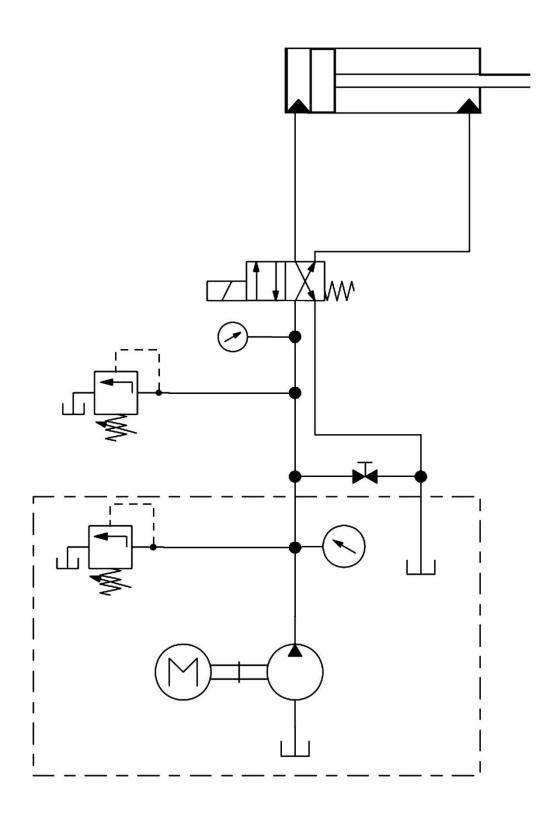
1. Number the elements of the circuit and state the names and function of the circuit parts in the following table

No.	Name	Function
1		
2		
3		
4		
5		
6		
7		
8		
9		
10		
11		
12		
13		
14		



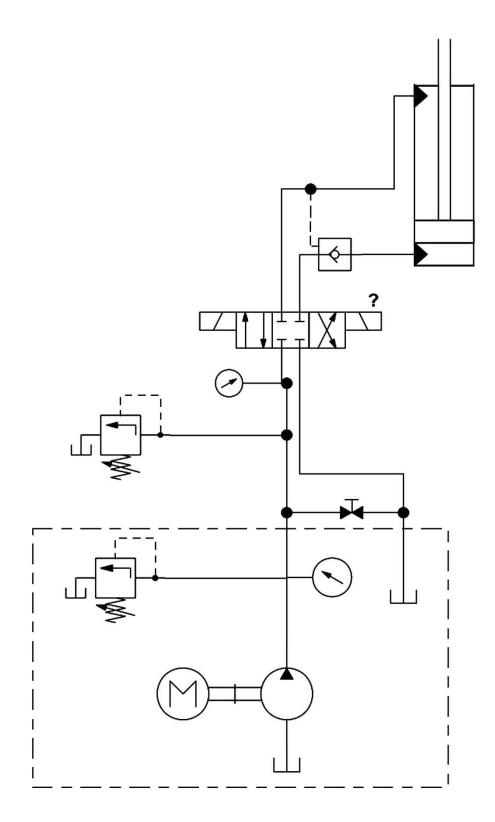
1. Number the elements of the circuit and state the names and function of the circuit parts in the following table

No.	Name	Function
1		
2		
3		
4		
5		
6		
7		
8		
9		
10		
11		
12		
13		
14		



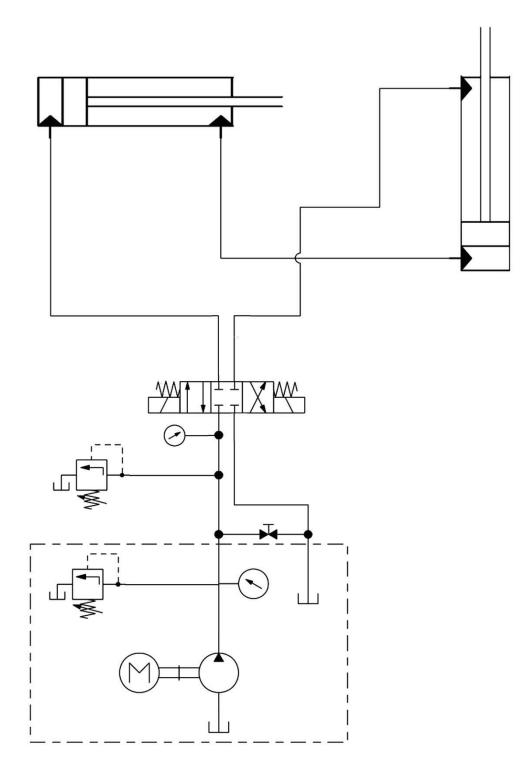
1. Number the elements of the circuit and state the names and function of the circuit parts in the following table

No.	Name	Function
1		
2		
3		
4		
5		
6		
7		
8		
9		
10		
11		
12		
13		
14		



1. Number the elements of the circuit and state the names and function of the circuit parts in the following table

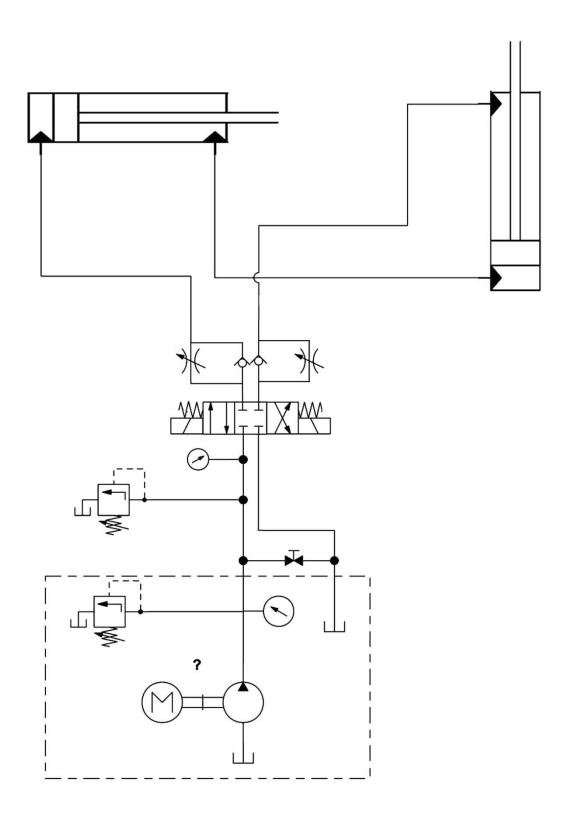
No.	Name	Function
1		
2		
3		
4		
5		
6		
7		
8		
9		
10		
11		
12		
13		
14		





1. Number the elements of the circuit and state the names and function of the circuit parts in the following table

No.	Name	Function
1		
2		
3		
4		
5		
6		
7		
8		
9		
10		
11		
12		
13		
14		



Hydraulic circuit No.7

1. Number the elements of the circuit and state the names and function of the circuit parts in the following table

No.	Name	Function
1		
2		
3		
4		
5		
6		
7		
8		
9		
10		
11		
12		
13		
14		

Modern Academy for Engineering & Technology



Practical Exam Questions

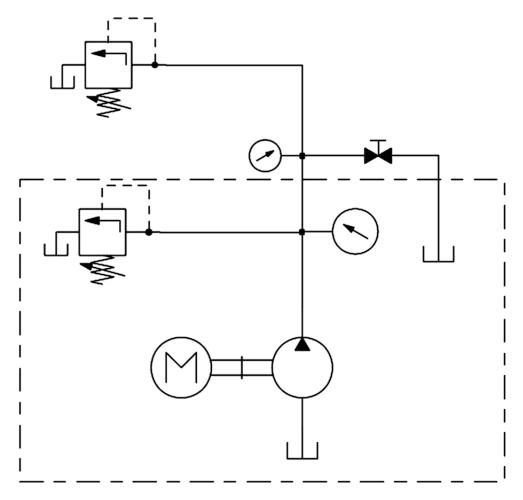
Modern Academy for Engineering & Technology



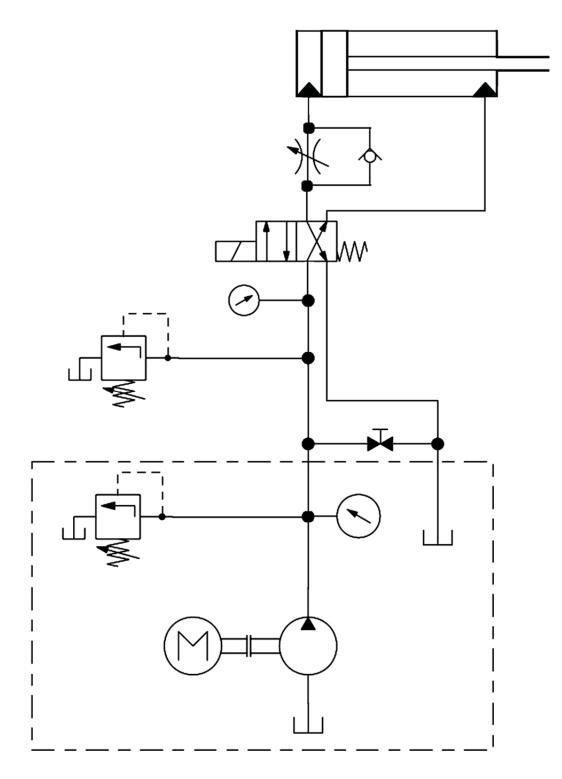
M 578 Fluid Power Engineering

Questions for Practical Examination

Explain the construction and operation of the shown hydraulic system, assemble this system on the hydraulic training unit and adjust the maximum system pressure to be 35 bar.

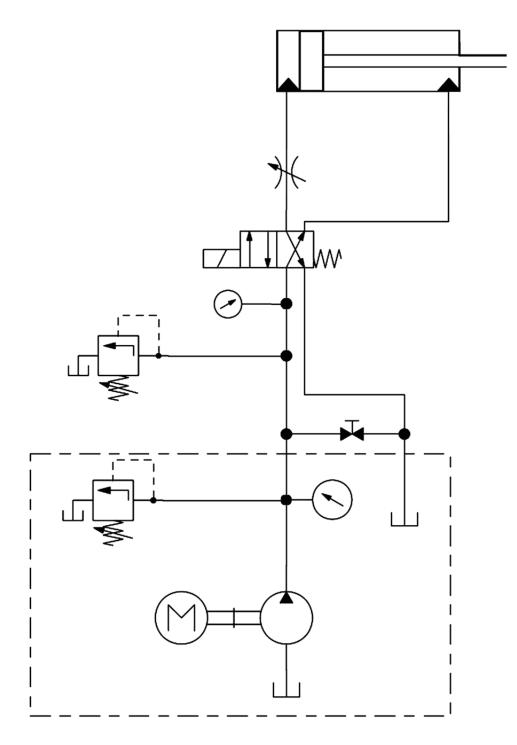


Explain the construction and operation of the shown hydraulic system, assemble this system on the hydraulic training unit and check its different operating modes.



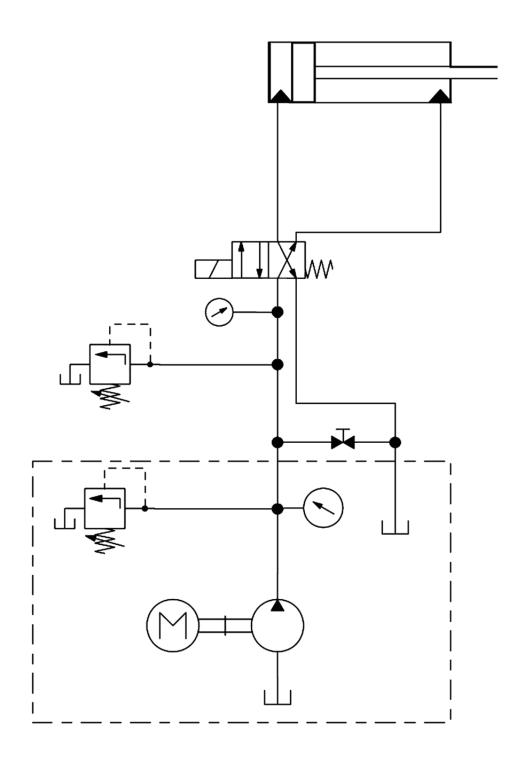
Hydraulic circuit No.2

Explain the construction and operation of the shown hydraulic system, assemble this system on the hydraulic training unit and check its different operating modes.

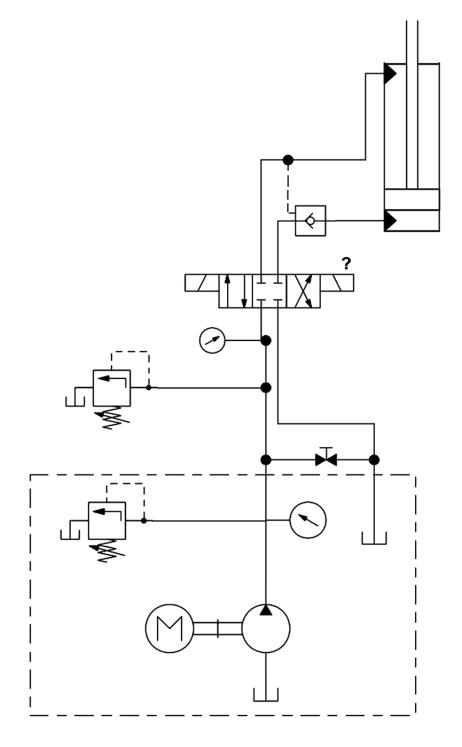


Hydraulic circuit No.3

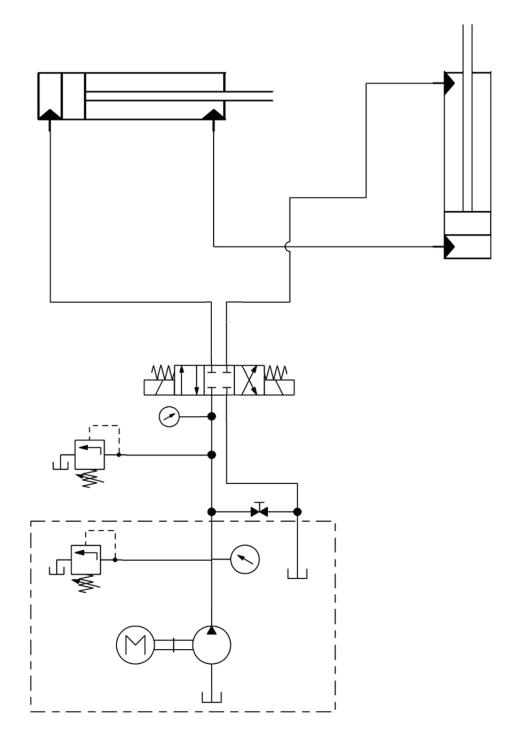
Explain the construction and operation of the shown hydraulic system, assemble this system on the hydraulic training unit and check its different operating modes.



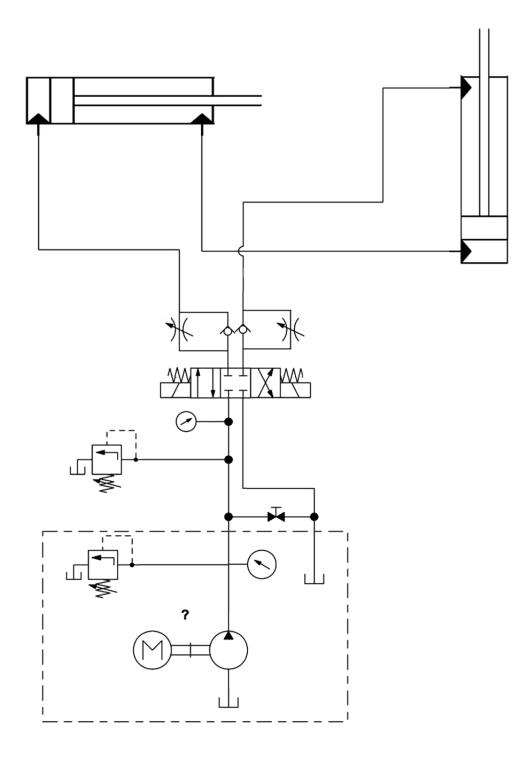
Explain the construction and operation of the shown hydraulic system, assemble this system on the hydraulic training unit and check its different operating modes.



Explain the construction and operation of the shown hydraulic system, assemble this system on the hydraulic training unit and check its different operating modes.



Explain the construction and operation of the shown hydraulic system, assemble this system on the hydraulic training unit and check its different operating modes.



Explain the construction and operation of the shown Centrifugal pump test stand. Put the system in operation and measure the pumping head and corresponding pump flow rate for two different points, then, give a comment on the measured results.



- Explain the construction and operation of the shown displacement pumps test stand.
- Explain the visualization of cavitation at the pump inlet line.
- Run the system and show the cavitation at the pump inlet line
- Discuss the origin of this phenomenon, its effects and how to avoid its occurrence.



- Explain the construction and operation of the shown displacement pumps test stand.
- Put the system in operation and measure the pumping flow rate for two different values of pump exit pressure, then, give a comment on the measurement results.



Academic Year: 2015-2016

✓	Mid-term exam paper
\checkmark	Model answer for the mid-term exam
NR	Corrective exam paper
NR	Model answer for the corrective exam
\checkmark	Final written exam paper
\checkmark	Model answer for the final written exam
✓	Final written exam evaluation and exam result analysis
x	Students course-questionnaire analysis, the file box contains a hard copy of this document
NR	November exam paper
NR	Model answer for November written exam
✓	Annual course report

✓=Document Exists x=Document doesn't exist NR=Not Relevant

Modern Academy

for Engineering and Technology in Maadi Manufacturing Engineering and Production Technology Department



Academic Year 2 Semester 1 Exam Date

2015-2016 First 17/11/2015

QUESTIONS FOR THE MID TERM WRITTEN EXAM					
Subject:	Subject: (M578) Hydraulic Power Systems Spec.: 5 th Man. Eng. & Prod. Tech.				
Examiners:	Examiners: Professor M. Galal RABIE & Dr Metwally Hussein		Time:	90 min	
Number of Pages: 1 Num		Number of Questions: 3		Attempt all questions	

Question 1

(8 points)

- (a) Draw the circuit of a simple hydraulic system, including a pump, directional control valve, hydraulic cylinder, relief valve, and other hydraulic components. State the function of the individual elements.
- (b) Define the bulk modulus of oil and calculate the shift of the piston in the given system if the force F is increased by 100 kN, given:

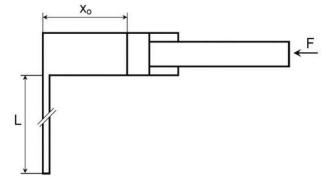
Piston area $A_p = .0176 \text{ m}^2$

Pipe line diameter d = 13 mm

Fluid bulk modulus B = 1.4GPa,

Initial displacement $x_0 = 0.5$ m,

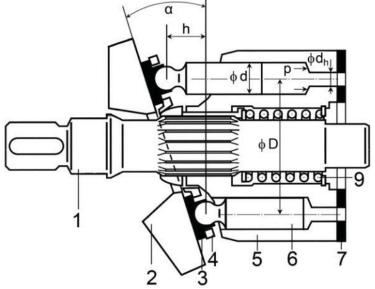
Pipe length L = 5 m,



Question 2

(8 points)

- (a)Derive an expression for the pressure and power losses in a hydraulic transmission line of constant diameter in the case of laminar flow.
- (b)Shown is a schematic of a displacement pump. Explain briefly its function and give an expression for its geometric volume.



Question 3

(4 points)

Give the expressions describing ideal and real displacement pumps, giving the meaning and units of the used symbols.

Give the meaning and units of all of the used symbols. The neatness and good organization of your exam paper are evaluated GOOD LUCK

Modern Academy

for Engineering and Technology in Maadi Manufacturing Engineering and Production Technology Department



Academic Year Semester Exam Date

2015-2016 First 17/11/2015

 MODEL ANSWER FOR THE MID TERM WRITTEN EXAM

 Subject:
 (M578) Hydraulic Power Systems
 Spec.:
 5th Man. Eng. & Prod. Tech.

 Examiners:
 Professor M. Galal RABIE & Dr Metwally Hussein
 Time:
 90 min

 Number of Pages:
 Number of Questions: 3
 Attempt all questions

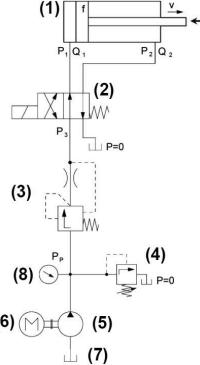
Question 1

(8 points)

(a) Draw the circuit of a simple hydraulic system, including a pump, directional control valve, hydraulic cylinder, relief valve, and other hydraulic components. State the function of the individual elements.

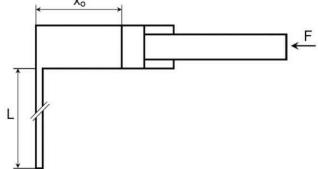
One of the possible answers

- (1) Hydraulic cylinder: Converts the hydraulic power to mechanical power. The input flow rate is converted to the piston speed while the input pressure is converted to the force which drives the load.
- (2) Directional control valve: Controls the direction of motion of the cylinder.
- (3) Series pressure compensated flow control calve: controls the flow rate, concequently the cylinder speed is controlled.
- (4) Relief valve, limiting the maximum system pressure.
- (5) Fixed displacement pump: Converts the mechanical power into hydraulic power.
- (6) Electric motor: drives the pump, by bsupplying the required mechanical power.
- (7)Hydraulic tank: locates the needed hydraulic liquid.
- (8) Pressure gauge: Indicates the system pressure.



(b) Define the bulk modulus of oil and calculate the shift of the piston in the given system if the force F is increased by 100 k, given: Piston area A_p = .0176 m²

Pipe line diameter d = 13 mm Fluid bulk modulus B = 1.4GPa, Initial displacement x_0 = 0.5 m, Pipe length L = 5 m,



The liquid compressibility is defined as the ability of liquid to change its volume when its pressure varies. For pure liquid, the relation between the oil volume and pressure variations is described by the following formula.

$$B = -\frac{\Delta P}{\Delta V / V} = -\frac{dP}{dV / V} \quad \text{or} \quad \frac{B}{V} = -\frac{dP}{dV} = -\frac{dP}{dt} / \frac{dV}{dt} \quad (2.48)$$

where ΔP = Pressure variation, Pa

 ΔV = Change in volume due to pressure variation, m³

- V = Initial oil volume, m^3
- B = Bulk modulus of oil, typically B = 1 to 2 GPa

$$\therefore B = -\frac{\Delta P}{\Delta V / V}$$

$$\therefore \Delta V = \frac{\Delta P}{B} V$$

$$\Delta P = \frac{F}{A_p}$$

$$\Delta P = \frac{100 \times 10^3}{0.0176} = 5.68 MPa$$

$$V = A_p x_o + \frac{\pi}{4} d^2 L = 0.0176 \times 0.5 + \frac{\pi}{4} \times 0.013^2 \times 5 = 9.463 \times 10^{-3} \text{ m}^3$$

$$\Delta V = \frac{5.68 \times 10^6}{1.4 \times 10^9} \times 9.463 \times 10^{-3} = 3.84 \times 10^{-5} \text{ m}^3$$

And $\Delta V = zA_p$

$$z = \frac{\Delta V}{A_p} = \frac{3.84 \times 10^{-5}}{0.0176} = 2.18 \text{ mm}$$

(8 points)

(a)Derive an expression for the pressure and power losses in a hydraulic transmission line of constant diameter in the case of laminar flow.

In hydraulic transmission lines, the flow may be laminar or turbulent depending on the ratio of the inertia forces to the viscous friction forces. This ratio is evaluated by the Reynolds number, Re. For laminar flow, Fig.2.4, the pressure losses in the line are calculated from the following relation, Appendix 2B.

$\Delta P = \lambda \frac{L}{D} \frac{\rho v^2}{2}$	(2.4)
$v = 4Q / \pi D^2$	(2.5)
$\lambda = 64/\text{Re}$	(2.6)
Re = $vD/v = \rho vD/\mu$	(2.7)
e D = Inner pipe diameter, m.	

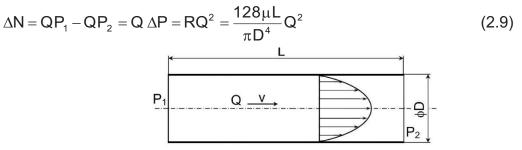
where

- L = Pipe length, m
- **Reynolds** number Re =
- Mean fluid velocity, m/s v =
- Pressure losses in the pipe line, Pa ΔP =
- λ = Friction coefficient for laminar flow
- ρ= Oil density, kg/m³

The following expression for the pressure losses ΔP was obtained by substituting Eqs. 2.5 to 2.7 in Eq.2.4.

$$\Delta \mathsf{P} = \frac{128\,\mu\mathsf{L}}{\pi\mathsf{D}^4}\mathsf{Q} = \mathsf{R}\,\mathsf{Q} \tag{2.8}$$

The term **R** expresses the resistance of the hydraulic transmission line. Its effect is equivalent to that of the electric resistance. Both of them dissipate energy and both are described by the same mathematical relation (e = Ri). The power loss ΔN in the pipeline is given by:



Laminar flow in pipeline

(b)Shown is a schematic of a displacement pump. Explain briefly its function and give an expression for its geometric volume.

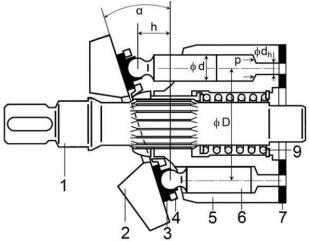


Figure 4.16 shows the construction and operation of a swash plate pump. The drive shaft **1** rotates and drives the cylinder block **5**. Both of the driving shaft and the cylinder block have the same axis of rotation. The cylinder block and its pistons **6**, rotate with the drive shaft. Each of the pistons is attached to a slipper pad **3**. The pistons and their slipper pads are inserted in the holes of the retaining plate **4**. Therefore, the retaining plate rotates with the pistons and the cylinder block. It is guided to rotate in a plane parallel to the swash plate **2**, by a fixed guide. The trajectory of the slipper pad is determined by the swash plate and the retaining plate. During rotation, each piston performs a reciprocating motion. During this process, a volume of fluid, corresponding to the piston area and stroke, is sucked or delivered via both control openings in the port plate **7**.

The cylinder block is pushed against the port plate by means of a spring **9**, which minimizes the leakage through the clearance separating them at the beginning of the pump operation. When the pressure builds up, it acts on the cylinder block by a tightening force given by { $0.25\pi(d^2 - d_h^2)P$ }. This force acts to the right, against the repulsion force due to the pressure distribution in the clearance between the cylinder block and the port plate. The resultant force acts to reduce this clearance and minimize the leakage through it. The pump geometric volume is given by the following expression:

$$V_g = \frac{\pi}{4} d^2 Dz \tan \alpha$$

(4.25)

where

d = Piston diameter, m. D = Pitch circle diameter, m

 α = Swash plate inclination angle, rad

Question 3

(4 points)

Give the expressions describing ideal and real displacement pumps, giving the meaning and units of the used symbols.

IDEAL PUMP

The pump **displacement** is defined as the volume of liquid delivered by the pump per revolution, assuming no leakage and neglecting the effect of oil compressibility. It depends on the maximum and minimum values of the pumping chamber volume, the number of pumping chambers and the number of pumping strokes per one revolution of the driving shaft. This volume depends on the pump geometry; therefore, it is also called **geometric volume** V_g . It is given by the following equation.

$$V_g = (V_{max} - V_{min})zi$$

Where i = Number of pumping strokes per revolution.

 $V_g =$ Pump displacement (geometric volume), m³/rev.

 V_{max} = Maximum chamber volume, m³.

 V_{min} = Minimum chamber volume, m³.

(4.1)

z = Number of pumping chambers.

Assuming ideal pump; with no internal leakage no friction and no pressure losses, the pump flow rate is given by the following expression.

$$Q_t = V_g n$$

where

 Q_t = Pump theoretical flow rate, m³/s. n = Pump speed, rev/s.

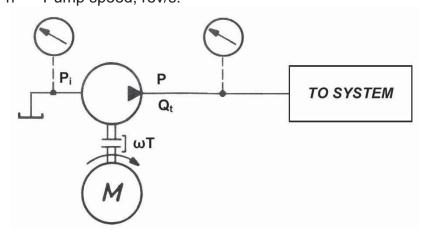


Fig.4.2 Typical displacement pump connection in hydraulic power circuits Following the assumption of ideal pump, the input mechanical power is equal to the increase in the fluid power as shown by the following equation, Fig.4.2.

$$2\pi nT_t = Q_t(P - P_i) = V_q n\Delta p \tag{4.3}$$

Or
$$T_t = \frac{V_g}{2\pi} \Delta P$$
 (4.4)
where $T_t =$ Pump theoretical driving torque, Nm.

 ΔP = Pressure increase due to pump action, Pa.

REAL PUMP

$\eta_{T} = \eta_{v} \eta_{m} \eta_{h}$	(4.11)
In the steady state operation, the real displacement pump is described by the following relations.	
$Q = V_g n \eta_v$	(4.12)
$N_h = N_m \eta_T$ Or $Q \Delta P = 2\pi nT \eta_T$	(4.13)
Then $T = \frac{V_g}{\Delta P}$	(4.14)

Ihen | = $\overline{2\pi}\eta_m\eta_h$

where

Total Efficiency η_T =

> Volumetric Efficiency = η_v

Mechanical Efficiency η_m

Hydraulic Efficiency η_h

(4.2)

Modern Academy

for Engineering and Technology in Maadi Manufacturing Engineering and Production Technology Department

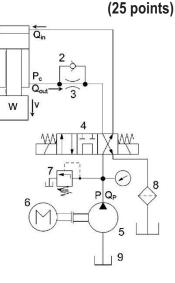


Academic Year Semester Exam Date 2015-2016 First 11/1/2016

	QUE	STIONS FOR THE FINAL WRIT	TEN EXA	M
Subject:	(M578) Hydraulic	Power Systems	Spec.:	5 th Man. Eng. & Prod. Tech.
Examiners:	Prof. M. Galal Rat	bie & Dr. Abdelmegid Abdellatif	Time:	3 hours
Numb	er of Pages: 2	Number of Questions: 4		Attempt all questions

Question 1

- (a) i. Give the names of each of the elements of the given system and explain the function of each of them.
 - ii. Explain the operation of the system in each of the positions of the directional control valve. Use short simple sentences.
 - iii. Calculate the pressure in the cylinder rod side Pc, the inlet flow rate Q_{in} , outlet flow rate Q_{out} , pump flow rate Q_P , pump output power N_h and area of the throttle valve At. Neglect the hydraulic losses in the system elements, except the throttle valve given: Pump exit pressure = 30 bar, piston speed = 0.07 m/s, piston area A_P = 78.5 cm², piston rod-side area A_r = 40 cm², oil density = 870 kg/m³, discharge coefficient = 0.611, the safety valve is pre-set at 350 bar and the weight of the body = 30 kN



- (b) i. State the function of the power systems.
 - ii. Discuss briefly the principle of operation of the hydraulic and electric power systems giving the advantages and disadvantages of hydraulic power systems. Draw the necessary schemes.

Question 2

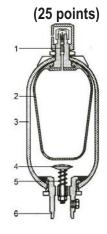
- a) i. Explain briefly the construction and operation of the given pump.
 - Write an expression for the geometric volume (displacement) of this pump, giving the meaning and units of all of the used symbols.

b) Calculate the displacement volume, input power, leakage flow rate, resistance to internal leakage and driving torque of a gear pump of the following parameters.

Pump speed =1450 rpm, number of teeth = 12, tooth module = 3.5 mm, Tooth width = 20 mm, pressure angle = 20° , inlet pressure = 0.2 MPa, exit pressure = 15 MPa, mechanical efficiency = 0.85 and volumetric efficiency = 0.9. Calculate the volumetric efficiency if the pressure is increased to 220 bar.

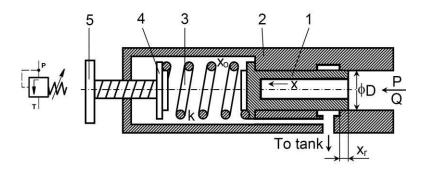
Question 3

- a) i. Explain the construction and operation of the given accumulator.
 - ii. Define the volumetric capacity of hydraulic accumulator.
 - iii. Derive an expression for the accumulator volumetric capacity.



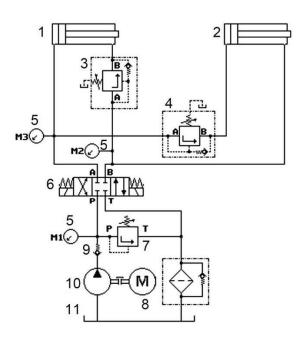
(25 points)

- **b)** i. Explain the construction and operation of the shown valve.
 - ii. Derive an equation for the valve flow rate then draw and discuss its flow-pressure characteristics. Explain how to reduce the over-ride pressure.



Question 4

- a) State the applications of hydraulic accumulators in hydraulic systems.
- b) Write the equations describing the steady state operation of hydraulic motors.
- c) Explain the construction and operation of the given hydraulic circuit.



Give the meaning and units of all of the used symbols. The neatness and good organization of your exam paper are evaluated GOOD LUCK

(25 points)

Modern Academy

for Engineering and Technology in Maadi Manufacturing Engineering and Production Technology Department



Academic Year 2 Semester F Exam Date 1

Qin

W

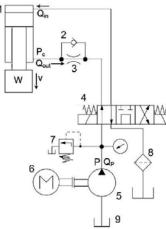
2015-2016 First 11/1/2016

MODEL ANSWER FOR THE FINAL WRITTEN EXAM Subject: (M578) Hydraulic Power Systems Spec.: 5th Man. Eng. & Prod. Tech. Examiners: Prof. M. Galal Rabie & Dr. Abdelmegid Abdellatif Time: 3 hours Number of Pages: 2 Number of Questions: 4 Attempt all questions

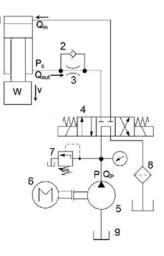
Question 1

- (a) i. Give the names of each of the elements of the given system and explain the function of each of them.
 - 1. Single-rod double-acting hydraulic cylinder, converts the hydraulic power into mechanical power. It acts to lift and lower the driven load.
 - 2. Check valve, allows for free fluid flow into hydraulic cylinder and prevents the flow in the opposite direction.
 - 3. Throttle valve, restricts the fluid flow.
 - 4. 4/3 directional control valve. Controls the direction of motion of hydraulic cylinder.
 - 5. Pump, Converts the mechanical power into hydraulic power.
 - 6. Electric motor, drives the pump.
 - 7. Relief valve, limiting the maximum operating pressure.
 - 8. Hydraulic filter, filters the hydraulic oil returning to tank
 - 9. Hydraulic tank, locates the operating oil.

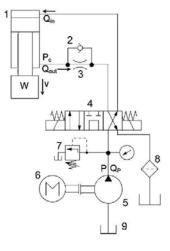
ii. Explain the operation of the system in each of the positions of the directional control valve. Use short simple sentences.



The oil flow from the pump to the DCV, then freely throuch the check valve, into the rodside of the cylinder. The oiston moved upwards, lifting the load. Then, the oil flows from the piston sidr, thru the DCV and filter, to the hydraulic tank.



In the neutral position, the DCV closes the cylinder ports, traping the oil in the cylinder and holding the load position. It by-passes the pump, minimizing the pump delivery pressure.



The fluid flows from the pump to the piston chamver. The cylinder extends, lowering the load. The oil returning from the cylinder rod-side flows throurg the throttle valve to the DCV, filter, to the tank. The throttling element creates the necessary back pressure which supports the load. It controlls the oilo flow rate, and consequently the load lowering speed.

(25 points)

9

iii. Calculate the pressure in the cylinder rod side P_c , the inlet flow rate Q_{in} , outlet flow rate Q_{out} , pump flow rate Q_P , pump output power N_h and area of the throttle valve A_t . Neglect the hydraulic losses in the system elements, except the throttle valve given: Pump exit pressure = 30 bar, piston speed = 0.07 m/s, piston area $A_P = 78.5$ cm², piston rod-side area $A_r = 40$ cm², oil density = 870 kg/m³, discharge coefficient = 0.611, the safety valve is pre-set at 350 bar and the weight of the body = 30 kN

$$\begin{split} &\mathsf{P}_{\rm c} = \left(\mathsf{W} + \mathsf{PA}_{\rm p}\right) / \mathsf{A}_{\rm r} = 13.4 \text{MPa} \\ &\mathsf{Q}_{\rm p} = \mathsf{vA}_{\rm p} = 0.00055 \text{m}^3 \, / \, \text{s} \\ &\mathsf{Q}_{\rm in} = \mathsf{Q}_{\rm p} = 0.00055 \text{m}^3 \, / \, \text{s} \\ &\mathsf{Q}_{\rm out} = \mathsf{vA}_{\rm r} = 0.00028 \text{m}^3 \, / \, \text{s} \\ &\mathsf{A}_{\rm t} = \mathsf{Q}_{\rm out} \, / (\mathsf{C}_{\rm d} \sqrt{2\mathsf{P}_{\rm c} \, / \, \rho}) = 2.6\,1 \text{mm}^2 \\ &\mathsf{N}_{\rm h} = \mathsf{PQ}_{\rm p} = 1649 \text{W} \end{split}$$

	Input	Name	Output
	30000	W	
	3000000	Р	
	.00785	Ар	
	.004	Ar	
	.07	v	
	.611	Cd	
Rule	870	ro	
Pc=(W+P*Ap)/Ar		Pc	13387500
Qp=v*Ap		Qp	.0005495
Qin=Qp		Qin	.0005495
Qout=v*Ar		Qout	.00028
At=Qout/(Cd*(2*Pc/ro)^0.5)		At	2.61223E-6
Nh=P*Qp		Nh	1648.5

(b) i. State the function of the power systems.

The power systems are used to transmit and control power.

ii. Discuss briefly the principle of operation of the hydraulic and electric power systems giving the advantages and disadvantages of hydraulic power systems. Draw the necessary schemes.

Electrical Power Systems

Electrical power systems solve the problems of power transmission distance and flexibility, and improve the controllability. Figure 1.4 illustrates the principal of operation of electrical power systems. These systems have the advantages of high flexibility and very long power transmission distance. But they produce mainly rotary motion. Rectilinear motion, of high power, can be obtained by converting the rotary motion into rectilinear motion by using suitable gear system or by using a drum and wire. However, holding the load position requires special braking system.

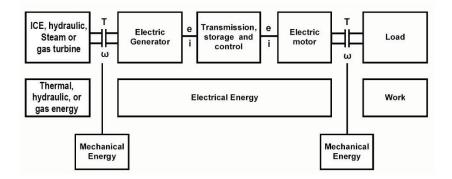


Fig.1.4 Power Transmission in Electrical Power System

Hydraulic Power Systems

In the hydrostatic power systems, the power is transmitted by increasing mainly the pressure energy of liquid. These systems are widely used in industry, mobile equipment, aircrafts, ship control ...etc. This text deals with the hydrostatic power systems, which are commonly called **hydraulic power systems**.

The function of this system is summarized in the following.

- 1. The prime mover supplies the system with the required mechanical power. The pump converts the input mechanical power to hydraulic power.
- 2. The energy-carrying liquid is transmitted through the hydraulic transmission lines; pipes and hoses. The hydraulic power is controlled by means of valves of different types. This circuit includes three different types of valves, a pressure control valve, a directional control valve and a flow control (throttle-check) valve.
- 3. The controlled hydraulic power is communicated to the hydraulic cylinder (or motor) which converts it to the required mechanical power. Generally, the hydraulic power systems provide both of rotary and linear motions.

Figure 1.8 gives the principal of operation of such systems.

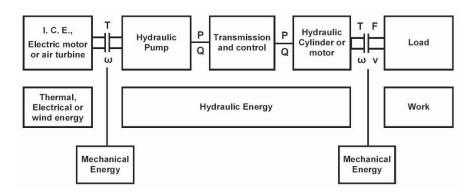


Fig.1.8 Power Transmission in hydraulic Power System

1.4 ADVANTAGES OF HYDRAULIC SYSTEMS

The main advantages of the hydraulic power systems are the following.

- 1. High power to weight ratio.
- 2. Self lubrication.
- 3. There is no saturation phenomenon in the hydraulic systems compared with saturation in electric machines. The maximum torque of electric motor is proportional to the electric current, but it is limited by the magnetic saturation.
- 4. High force to mass ratio, and torque to inertia ratio, which result in high acceleration capability and rapid response of the hydraulic motors.
- 5. High stiffness of the hydraulic cylinders, which allows stopping loads at any intermediate position.
- 6. Simple protection against overloading.
- 7. Possibility of energy storage in hydraulic accumulators.
- 8. Flexibility of transmission compared with mechanical systems.
- 9. Availability of both of rotary and rectilinear motions.
- 10. Safe regarding the explosion hazard.

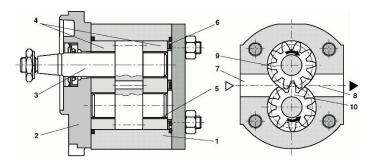
The hydraulic power systems have the following disadvantages.

- 1. The hydraulic power is not readily available, as the electrical one. Hydraulic generators are therefore required.
- 2. High cost of production due to the requirements of small clearances and high precision production process.
- 3. High inertia of transmission lines which increases their response time.
- 4. Limitation of the maximum and minimum operating temperature.
- 5. Fire hazard when mineral oils are used.
- 6. Problems of oil filtration.

Question 2

(25 points)

i. Explain briefly the construction and operation of the given pump.



1. Housing, 2. Mounting flange, **3.** Drive shaft, 4. Two bearing blocks, side plates, 5. Bearing bush, 6. Discs, 7&8. Inlet and exit ports, 9. Driving gear, 10. Driven gear

Gear pumps are of multi-rotor displacement type. There are four main types of gear pumps; external gear pumps, internal gear pumps, screw pumps and gerotors. The External gear pumps, Fig.4.22, consist of the housing 1, mounting flange 2, drive shaft 3, two side plates, 4, bearing bush 5, two gears 9&10 and disc 6. The driving gear 9 is connected to the driving shaft 3. The pumping chamber is formed by the surfaces of two adjacent teeth, the inner surface of housing and the two side plates. During the rotational movement of the gears, the un-meshing gears release the pumping chambers. The resulting under pressure, together with the pressure in the suction line, forces the fluid to flow to the pump inlet port 7. This fluid fills the pumping chambers, then, it is moved with the rotating gear from the suction side to the pressure side. Here the gears mesh once more and displace the fluid out of the pumping chambers and prevent its return to the suction zone.

ii. Write an expression for the geometric volume (displacement) of this pump, giving the meaning and units of all of the used symbols.

In the case of external gear pump with two spur gears, the pump geometric volume is given by the following relation.

(4.30)

$$V_{a} = 2\pi bm^{2}(z + \sin^{2}\gamma)$$

b = Tooth length, m m = Module of tooth, m z = Number of teeth per gear γ = Pressure angle of tooth, rad V_g = Pump displacement, m³/rev

b) Calculate the displacement volume, input power, leakage flow rate, resistance to internal leakage and driving torque of a gear pump of the following parameters.

Pump speed =1450 rpm, number of teeth = 12, tooth module = 3.5 mm, Tooth width = 20 mm, pressure angle = 20° , inlet pressure = 0.2 MPa, exit pressure = 15 MPa, mechanical efficiency = 0.85 and volumetric efficiency = 0.9. Calculate the volumetric efficiency if the pressure is increased to 220 bar.

$$\begin{split} V_{g} &= 2\pi bm^{2}(z+sin^{2}\gamma) = 1.865 \times 10^{-5}m^{3}\\ Q_{t} &= V_{g}n = 4.51 \times 10^{-4}m^{3} \,/\,s\\ Q &= Q_{t}\eta_{v} = 4.06 \times 10^{-4}m^{3} \,/\,s\\ T &= \frac{V_{g}}{2\pi\eta_{m}\eta_{h}}(Po-Pi) = 51.69Nm\\ N_{in} &= 2\pi nT = 7.848kW\\ Nh &= P_{o}Q = 6.085kW\\ Q_{L} &= Qt-Q = 4.51 \times 10^{-5}m^{3} \,/\,sm^{3} \,/\,s \end{split}$$

$$R_{L} = (P_{o} - P_{i})/Q_{L} = 3.28 \times 10^{11}$$
$$\sigma = \frac{\pi^{2} \cos^{2} \gamma}{4(z+1)} = 16.8\%$$

The volumatric efficiency at 220 bar is:

$$\eta_{v220} = 1 - \frac{220 \times 10^5}{R_L V_G n} = 0.851$$

Rules	-	Va	riables		
Status Rule	Sta	tus	Input	Name	Output
* Unsat gama=20*pi()/180			12	z	
* Unsat Vg=2*pi()*b*m*m*(z+(sin(gama))^2)			24.1666667	n	
* Unsat Qt=Vg*n			.9	etav	
* Unsat Q=Qt*etav			.85	etam	
* Unsat T=(Po-Pi)*Vg/(2*pi()*etam*etah)			15000000	Po	
* Unsat Nin=2*pi()*n*T			.02	b	
* Unsat Nh=Po*Q			.0035	m	
* Unsat QL=Qt-Q			1	etah	
* Unsat RL=(Po-Pi)/QL			200000	Pi	
* Unsat etav220=1-2.2e7/(RL*Vg*n)				gama	.34906585
				Vg	1.86526E-5
				Qt	.000450772
				Q	.000405695
				Т	51.6896017
				Nin	7848.73752
				Nh	6085.42318
				QL	4.50772E-5
				RL	3.28326E11
				etav220	.851351351

Question 3

(25 points)

a) i. Explain the construction and operation of the given accumulator.

In this class of accumulators, a bladder is used as the elastic separation of the oil and compressed gas. The bladder is fastened inside the steel body by means of the vulcanized gas-charging valve assembly. It can be removed and replaced through an opening in the steel body at the oil-valve assembly. Initially, the bladder is charged with compressed gas while the oil port is drained. The bladder is stretched until it comes in contact with the vessel walls.

The bladder material withstands high compression stresses, but its resistance to shear and tensile stresses is very low. Therefore, the bladder is protected against extruding through the oil connection port by one of two different ways:

- Closing the oil port by a hemispherical steel plate with great number of small diameter holes allowing for free oil flow. The holes diameter is too small that the resulting shear stress acting on the bladder walls is less than the allowable value.
- Using a mushroom shaped protection valve which seats when the bladder is precharged.

When pumping the oil to the accumulator at pressures higher than the pre-charge pressure, the oil enters the accumulator, compressing the gas and reducing the bladder volume. The internal tightness of the bladder accumulator is perfect as long as the bladder is not damaged.

ii. Define the volumetric capacity of hydraulic accumulator.

The volumetric capacity of accumulator; V_a is defined as the volume of oil delivered to/from the accumulator at pressure P in the operating range; $P_1 \le P \le P_2$.

iii. Derive an expression for the accumulator volumetric capacity.

The following equation describes the gas compression process.

$$P_{o}V_{o}^{n} = P_{1}V_{1}^{n} = P_{2}V_{2}^{n} = const$$
 (6.2)

According to the type of compression process, the value of the exponent **n** varies in the range from 1 to 1.4. For isothermal process, n=1, for polytropic process, 1<n<1.4 and for adiabatic process, n= γ =1.4. The pressure is absolute, whenever a gas process is considered. If the compression process is so slow that the gas temperature is kept constant, the process is isothermal and the gas pressure and volume are related by the following relation.

$$P_{o}V_{o} = P_{1}V_{1} = P_{2}V_{2} = Const.$$
 (6.3)

$$V_{a} = V_{1} - V_{2} = V_{o} \left\{ \left(\frac{P_{o}}{P_{1}} \right)^{\frac{1}{n}} - \left(\frac{P_{o}}{P_{2}} \right)^{\frac{1}{n}} \right\}$$
For polytropic process (6.4)

$$V_{a} = V_{1} - V_{2} = V_{o} \left\{ \left(\frac{P_{o}}{P_{1}} \right) - \left(\frac{P_{o}}{P_{2}} \right) \right\}$$
 For isothermal process (6.5)

Where,

P_o =Accumulator charging pressure, gas pressure, Pa (abs)

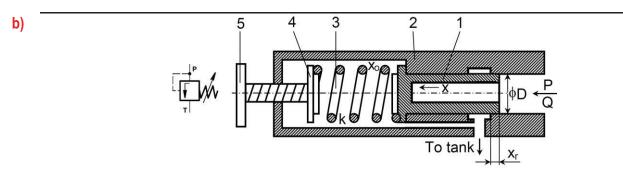
P₁ =Minimum system pressure, Pa (abs)

P₂ =Maximum system pressure, Pa (abs)

V_o =Accumulator size, volume of charging gas at pressure P_o, m³

 V_1 =Volume of gas at pressure P₁, m³

V₂ =Volume of gas at pressure P₂, m³



i. Explain the construction and operation of the shown valve

This is a direct operated relief valve. The Poppet 1 is acted on by the spring 3. The pre0compression distance of the spring is pre-set by the rotating handle 5. Initially, the poppet rests against the hosing 2 shoulder. It disconnects the inlet port from the tank port. As the pressure P increases, the pressure force acting on the poppet increases ($F_p=\pi$ D²P/4). As the pressure force F overcomes the spring force kx_o , the poppet starts to move to the left. When the pressure P equals the cracking pressure P_r, the popper should have displaced by x_r as {P_r=k(x_o+x_r)*4/(π D²}. For pressures greater than P_r, the valve opens, allowing the oil from the high-pressure port to flow to the tank.

ii. Derive an equation for the valve flow rate then draw and discuss its flow-pressure characteristics. Explain how to reduce the over-ride pressure.

Considering the valve shown in Fig.5.2, the relation between the valve flow rate and system pressure is deduced in the following.

$$P_{r} = \frac{k}{A_{P}} (x_{o} + x_{r})$$
(5.2)

Then

$$x_{r} = P_{r} \frac{A_{P}}{k} - x_{o} \quad \text{Or} \quad x_{o} + x_{r} = \frac{A_{P}}{k} P_{r}$$

$$A_{P} = \pi D^{2} / 4 \qquad (5.3)$$

Neglecting the spool radial clearance leakage, then;

$$Q = \begin{cases} 0 & \text{for } x \le x_r, \qquad A_v = 0 \\ \\ C_d A_v \sqrt{2P / \rho} & \text{for } x > x_r, \qquad A_v = \omega(x - x_r) \end{cases}$$
(5.5)

In the steady state, the valve poppet becomes in equilibrium under the action of the pressure forces, spring force and jet reaction forces. Neglecting the jet reaction forces and assuming zero return line pressure, then when the pressure increases such that the spool displaces by a distance x;

$$PA_{P} = k(x_{o} + x)$$
 Then $x = P\frac{A_{P}}{k} - x_{o}$ (5.6)

$$A_{v} = \omega \left(P \frac{A_{P}}{k} - x_{o} - x_{r} \right) \qquad \text{Or} \qquad A_{v} = \omega \frac{A_{P}}{k} \left(P - P_{r} \right)$$
(5.7)

Then

$$Q = C_{d} \omega \frac{A_{P}}{k} (P - P_{r}) \sqrt{2P/\rho} = K(P - P_{r}) \sqrt{P}$$
(5.8)

$$K = C_{d} \omega \frac{A_{P}}{k} \sqrt{2/\rho}$$
(5.9)

Av =Valve throttling area, m²

C_d =Discharge coefficient.

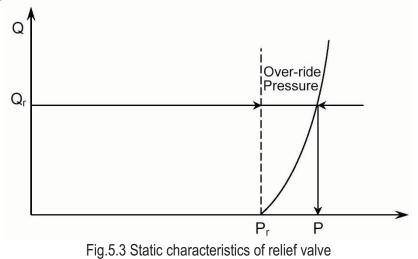
P =Valve input pressure, Pa.

x =Spool displacement, m

x_r =Spool overlap, m

 ω =Valve throttling area proportionality coefficient, m.

The steady state characteristics of the valve are described by the pressure-flow rate relation, shown in Fig.5.3. This figure shows that the maximum pressure P, corresponds to the relieved flow rate Q_r . The pressure difference (P–P_r) is called the over-ride pressure. At a pressure P=P_r, the poppet is in equilibrium under the action of the pressure and spring pre-compression forces. The valve is closed and its flow rate is zero, assuming no leakage. In order to allow the oil to flow, the poppet should displace, which takes place at pressures higher than P_r. This increase in pressure is the over-ride pressure. For higher flow rates, the over-ride pressure is higher.



The over-ride pressure could be decreased by increasing the slope of the flow-pressure curve, by increasing

the value of parameter H; $K = C_d \omega \frac{A_P}{k} \sqrt{2/\rho}$. This could be achieved by increasing the value

dimensions and decreasing the spring stiffness.

Question 4

(25 points)

(7.16)

)

- a) State the applications of hydraulic accumulators in hydraulic systems.
 - **1. a)** Reserve source of energy
 - **b)** Compensation of the short duration large flow demands; to reduce the required pump size and the driving power.
 - c) Pump unloading.
 - **d)** Reducing the response time of actuators placed at long distance from the pump.
 - 2. Maintaining constant pressure; compensation for leakage losses
 - 3. Thermal compensation
 - 4. Smoothing of the pressure and flow pulsation
 - 5. Load suspension on load transporting vehicles
 - 6. Absorption of hydraulic shocks
 - 7. Hydraulic spring in the car suspension
- b) Write the equations describing the steady state operation of hydraulic motors.

The function of hydraulic motors is the reverse of that of the pump. Hydraulic motors are displacement machines converting the supplied hydraulic power into mechanical power. They perform continuous rotary motion. The displacement (or geometric volume) of a hydraulic motor is the volume of oil needed to rotate the motor shaft by one complete revolution. The motor speed depends on the flow rate, while the supply pressure depends mainly on the motor loading torque. In the case of an ideal motor with no leakage and no friction, the following relations are used.

$$n_{m} = Q_{t} / V_{m}$$

$$\Delta P = \frac{2\pi}{V_{m}} T$$
(7.13)
(7.14)

where

 n_m =Motor speed, rev/s ΔP =Applied pressure difference, Pa V_m =Geometric volume of motor, m³/rev T =Loading torque, Nm Q_t =Theoretical flow rate, m³ /s.

The theoretical motor flow rate is less than the real flow due to the internal leakage. The volumetric efficiency of motor is defined as follows.

$\eta_v = \frac{Q_t}{Q}$	(7.15)

Or $n_m = \frac{Q\eta_v}{V_m}$

$$Q\Delta P\eta_{T} = 2\pi n_{m}T$$
(7.17)

Then;
$$\Delta P = \frac{2\pi}{V_m \eta_m \eta_h} T$$
 (7.18)

where

Q =Real motor flow rate, m^3 / s

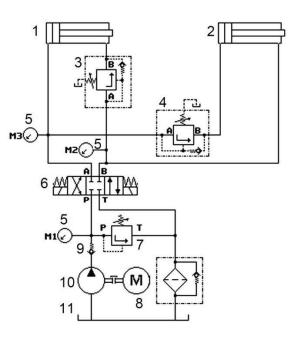
 η_T =Total motor efficiency

 η_m =Motor mechanical efficiency

 η_v = Motor volumetric efficiency

 η_h =Motor hydraulic efficiency

c) Explain the construction and operation of the given hydraulic circuit.



Components of the system:

1 and 2 hydraulic cylinders, 3 and4 sequence valves, 5 pressure gages, 6 4/3 directional control valve, 7 safety valve, 8 electric motor, 9 check valve, 10 pump and 11 hydraulic tank.

Operating modes

- 1. With DCV in the neutral position. All of the DCV ports are closed. The pump delivery line, being closed, forces the pump glow through the relief calve. The pump exit pressure is maximum.
- 2. With the DCV in the left position, Cylinder 2 retracts. The fluid flows from cylinder 2 to the tank through the check valves mounted in parallel to the sequence valve 4. When the cylinder 2 is stopped or its load increases to the level pre-set at the sequence valve 3, cylinder 1 will retract.
- 3. With the DCV in the right-hand position, cylinder 1 starts to extend. The sequence valve 4 is closed, preventing the pressurized oil supply from reaching cylinder 2. When cylinder 1 reaches its end position, or its load increases, causing the pressure to increase to the pre-set value on sequence valve 4, it opens. The pressurized oil reaches cylinder 2, which extends.

Give the meaning and units of all of the used symbols. The neatness and good organization of your exam paper are evaluated **GOOD LUCK** Ministry of Higher Education

For Engineering & Technology in

Maadi

Modern Acade

وزارة التعليم العالى الأكاديمية الحديثة للهندسة والتكنولوجيا بالمعادى

Written Examination and Written Examination Results Evaluation

1. Examination header: (should be according to the Modern Academy Format)

Modern Academy

for Engineering and Technology in Maadi Manufacturing Engineering and Production Technology Department

-	1		17	-
1	lode	an 1	nde	my
0	1000			1
		Since log3	1.10	maadi

Academic Year 2015-2016 Semester First Exam Date 11/1/2016

QUESTIONS FOR THE FINAL WRITTEN EXAM

Subject: (M578) Hydraulic Power Systems

Systems **Spec.:** 5th Man. Eng. & Prod. Tech.

Examiners: Prof. M. Gal	al Rabie & Dr. Abdelmegid Abdellatif	Fime: 3 hours
Number of Pages: 2	2 Number of Questions: 4	Attempt all questions

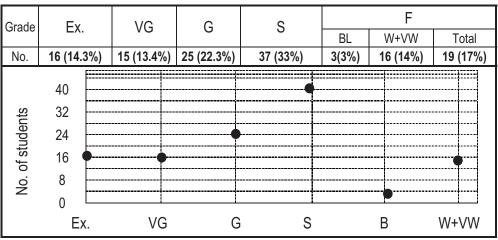
2. Evaluated ILO's

		Quest.1	Quest.2	Quest.3	Quest.4
Maxii	mum points	25	25	25	25
σ	Knowledge & understanding (a1 to a 6)	2,4, 5	2,4	2,4	2,4,5
Covered ILO's	Intellectual skills (b1 to b 3)	2,3	2,3	2,3	2,3,4
§ ⊒	Practical applied skills (c1 to c 5)	2	2	3	2
Ŭ	General transferrable skills (d1 to d 4)	2	2	2	2
Succ	ess %	89	83	68.8	60.7
Avera	age points%	72.5	67.6	58.8	54.6
Highe	est mark %	100	100	100	100
Lowe	est Mark %	28	0	0	0

3. Comment on the ILO's covered by the exam

- The exam paper header agrees with the MAM standard form
- The exam paper measures 73% of course ILO's measurable in written form and the variety of questions is practically balanced.
- The exam considers the course aims listed in the course specification.

4. Collective examination results



5. Comment on the Examination results and feedback

- The exam level is practically convenient, considering the percentage of success.
- Low success percentage in questions 3 and 4 may be attributed to low attendance during the second half of semester. Moreover, it implies the need to develop new plans to encourage the students, or oblige them, to attend the late term activities.
- The exam result shows considerable weakness in hand sketching and report writing and English language level.
- The exam showed acceptable level in manipulation with numbers. However, a non-negligible percentage of students suffer from poor comprehension of SI units and numbers evaluation.



Annual Course Report Academic year 2014-2015

A-Basic Information

- 1- Course Code & Title: (M578) Hydraulic Power Systems
- 2- Program(s) on which this course is given: Production Engineering and manufacturing

Technology BSc Program

- 3- Year/Level of program: Fourth Year/Second Semester
- 4- Credit hours

Total7hrsLectures3 hrsTutorial2 hrsPractical2 hr5- Names of lecturers contributing to the delivery of the course:Prof. Dr. M Galal Rabie

- 6- Course coordinator: Prof. Dr. M Galal Rabie
- 7- External evaluator: Non

B-Statistical Information

- 1- No. of students attending the course:
- 2- No. of students completing the course:
- 3- Results:

	No.	%
Passed	44	88
Failed	6	12

No.	53	100	%
No.	50	94	%

Grading of successful students:					
Grade	No.	%			
Excellent	0	0			
Very Good	8	18.2			
Good	14	31.8			
Pass	22	50			

C-Professional Information

1 – Course teaching

Торіс	Tota	l hours	Lecturers
Торіс	Plan.	Actual	Lecturers
Power systems, classification, operation, and comparison.	4		
Introduction to hydraulic power systems and standard symbols	10	semester a 20% was	
Hydraulic fluids; properties and their effect on the system performance.	4	°	
Hydraulic transmission lines and connectors	10		
Hydraulic pumps:	4	l thi: efor 's b'	
 Classification and basic mathematical relations 	4	uring this se Therefore, a hours bv 20	bie
Gear pumps, vane pumps and piston pumps	4		Rabie
 Fixed and variable displacement pumps and pump control 	4	ffective teaching weeks d 12 with total of 84 hours. ced reduction of teaching	Dr. M Galal
Control valves	4	g w 84	Ű
Classification and basic design		teaching total of 8 uction of	Dr. D
• Pressure control valves (direct/pilot operated); relief valves, pressure		tea tota uctic	
reducers, sequence valves and accumulator charging valves	6	live /ith red	Prof.
Directional control valves	4	effective 12 with	
Flow control valves	4	The ef were ` balanc	
Check valves	5	Th w∈ ba	
Hydraulic actuators; cylinders, motors and rotary actuators	2		
Accessories; accumulators, filters, reservoirs, pressure switches,etc	4		

Small project; design and analysis of the hydraulic system for an industrial			
application. Analysis of the possible operational problems	6		
Total hours	105	84	

<70%

- >90 % 70-90 % Topics taught as a percentage of the content specified: •
- Reasons in detail for not teaching any topic: Non
- If any topics were taught which are not specified, give reasons in detail: Non
- Achieved program intended learning outcomes, ILO's: Actually, all of the intended learning outcomes were achieved. The 20% obligatory cut of the net teaching hours was partially compensated by additional reports and seminars.

Knowledge & Understanding	Intellectual skills	Applied Skills	General transferable skills
a1 to a6	b1 to b3	c1 to c5	d1 to d4

2- Teaching and learning methods:

lecture, presentations & movies, discussions & seminars, tutorials, problem solving and self-learning, modeling

If teaching and learning methods were used other than those specified, give Non reasons:

Seminar/Workshop:

The following are two seminars arranged by 8 students and 13 Technical Reports by 66 students: Seminars

No.	Title	Number of students
1	Using Automation Studio in hydraulic system design	4
2	Using NFPA educational CD for training on hydraulic power systems	4
3	Reading data sheets of hydraulic elements	4
4	Using Water as a Hydraulic Liquid	3

Technical Reports

SN	Title	Number of students
1.	Displacement pumps	2
2.	Rotodynamic Pumps	2
3.	Pressure Control Valves	2
4.	Flow rate control valves	2
5.	Hydraulic cylinders	2
6.	Electric Motors	2
7.	Hydraulic Motors	2
8.	Hydraulic Motors	2

3- Student assessment:

Tools	To measure the content of	Time	Grading	%
		schedule		
Mid-Term Exam	a1 to a6, b1 to b3 and c1 to c4	sixth week	15	10
Term papers, quizzes and seminars	a1 to a5, b1 to b3, c1, c2 and c4 and d1 to d4	Bi-weekly	15	10
Practical exams	a3, c1 and c5	Fifteenth week	20	13.3
Written exam	a1 to a6, b1 to b3 and c1 to c4 and d2	16 th week	100	66.7
		Total	150	100

Members of examination committee: Role of external evaluator:

Dr. M. Galal RABIE and Dr. Abdelmegid Abdellatif

Non

4- Facilities and teaching materials:

Totally adequate	Yes
Adequate to some extent	
Inadequate	
Non	

List any inadequacies:

5- Administrative constraints (List any difficulties encountered)

> Non

6. Comment on the Examination results and feedback

* The exam paper header agrees with the MAM standard form

- * The exam paper measures 65% of course ILO's measurable in written form and the variety of questions is practically balanced.
- * The exam considers the course aims listed in the course specification.
- * The exam level is practically convenient, considering the percentage of success.
- * Low success percentage in questions 3 and 4 may be attributed to low attendance during the second half of semester. Moreover, it implies the need to develop new plans to encourage the students, or oblige them, to attend the late term activities.

* The exam result shows considerable weakness in hand sketching and report writing and English language level.

7- Student evaluation of the course:

	List any criticisms	Response of course team
(a)	Non	

8- Comments from external evaluator(s):

	Comment	Response of course team
(a)	Non	

9- Course enhancement:

Progress on actions identified in the previous year's action plan. State whether or not completed and give reasons for any non-completion:

◡.			
	Actions required	Planned Completion date	Accomplishment
	Non		

10- Action plan for academic year 2013 – 2014

A	ctions required	Completion date	Person responsible

Course coordinator:	Prof. Dr M Galal Rabie
Signature:	
Date:	July 24, 2015

The files are kept for five years in this box, then the older year's files are replaced

Academic Year: 2014-2015

Mid-term exam paper
Model answer for the mid-term exam
Corrective exam paper
Model answer for the corrective exam
Final written exam paper
Model answer for the final written exam
Final written exam evaluation and exam result analysis
Students course-questionnaire analysis
November exam paper
Model answer for November written exam
Annual course report

Academic Year: 2013-2014

Corrective exam paper
Model answer for the corrective exam
Final written exam paper
Model answer for the final written exam
Final written exam evaluation and exam result analysis
Students course-questionnaire analysis
November exam paper
Model answer for November written exam
Annual course report

Academic Year: 2012-2013

Corrective exam paper
Model answer for the corrective exam
Final written exam paper
Model answer for the final written exam
Final written exam evaluation and exam result analysis
Students course-questionnaire analysis
November exam paper
Model answer for November written exam
Annual course report

Academic Year: 2011-2012

Corrective exam paper
Model answer for the corrective exam
Final written exam paper
Model answer for the final written exam
Final written exam evaluation and exam result analysis
Students course-questionnaire analysis
November exam paper
Model answer for November written exam
Annual course report